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AIR FORCE BOOM EVENT ANALYZER RECORDER (BEAR): Comparison with NASA Boom Measurement System



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FOR THE COMMANDER

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PREFACE

This report was prepared by the Biodynamic Environment Branch, Armstrong Aerospace Medical Research Laboratory, under Project/Task 723134, Exploratory Noise and Sonic Boom Research with partial funding from the Noise and Sonic Boom Impact Technology (NSBIT) Advance Development Program Office under Project Number 3037.

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INTRODUCTION

As part of its exploratory noise and sonic boom research program, the Armstrong Aerospace Medical Research Laboratory (AAMRL) with its contractor, Systems Research Laboratory (SRL), designed and built a Sonic Boom Event Analyzer Recorder (BEAR) system. The intent of this development was to provide the Air Force with a readily portable, unmanned recording system which could efficiently and accurately monitor the acoustic environment and identify and record full sonic boom pressure-time signatures while rejecting unwanted noise events produced by subsonic aircraft, ground vehicles, gunfire, wind and other sources.

The BEAR system, which is described in the next section, was extensively checked and calibrated in the Laboratory during development. The purpose of the boom measurement program described in this report was to field-check twelve BEAR systems with actual sonic boom environments in order to verify their capabilities and establish their credibility over their full design range. Accordingly, AAMRL conducted tests at Edwards AFB, CA on 16-18 Sep 86 with the support and interest of NASA who simultaneously deployed their analog, manned, sonic boom recorder systems. The specific approach was to compare in detail the data gathered by the Air Force BEARs with those gathered by the NASA systems. This report documents the results of this test program.

DESCRIPTION OF TEST

AAMRL Full Signature Sonic Boom Recorder

The Boom Event Analyzer Recorder (BEAR) is a 16 bit microprocessor-based instrument that continuously samples the acoustic environment then captures and stores the digital waveform of any loud impulsive noise (Figure 1). The recorder can discern a sonic boom from the normal background noise and capture it in permanent solid state random access memory (RAM) storage for later analysis. The RAM modules can then be interfaced with a Data Retrieval Unit (DRU) and the information on the DRU transferred to a Zenith Z-100 microcomputer (Figure 2). The microcomputer displays each recorded event, time of occurrence and summary information for all the data stored.

The BEAR digitizes the noise environment at an 8 kHz sampling rate and analyzes it during the downtime between the sampling intervals giving it real-time screening for sonic boom events. The BEAR examines the event level, duration, pulse time and risetime to determine if it should be stored as a boom event. These parameters are selectable via the input keypad to make the BEAR a very flexible instrument with which to capture a wide variety of impulsive events. Along with setting the boom evaluation criteria, the keypad allows input of date, time, test number, location and serial number of the unit. This information is stored in the same RAM modules as data every time any parameter is changed. The operator can also select three other modes from this keypad: calibration, clear memory or data save. In the calibration mode the BEAR simply displays the root-mean-square level of two seconds of the input signal to the microphone for checking against a standard 124 dB sound pressure level, piston-phone calibrator. No data are saved to the RAM modules in this mode. The clear memory mode asks the operator to input a special code and, when entered, simply erases the RAM modules and runs the BEAR unit through the internal self-test routines that verify all the hardware components are working properly. The third mode allows the operator to collect one second of data with no screening. This allows the operator to collect and store background noise or the calibrator signal or anything that is desired. The BEAR has a frequency response of 0.5 Hz to 2,500 Hz for reproducing a sonic boom time history adequate for environmental impact analysis. The maximum overpressure the BEAR is designed for is 155.3 dB (24.4 pounds per square foot or 1170 pascal) with an 80 dB useable dynamic range. The RAM modules on a single unit have 512K bytes of memory allowing the BEAR to store over 100 "normal" sonic booms. The BEAR is designed to operate with a PCB-Piezo resistive microphone that is totally sealed and extremely rugged. This microphone is mounted inverted over an 18" diameter steel plate in a vibration isolation mount. A 4" diameter foam windscreen inside a 18" diameter inverted cone covers the microphone and provides wind noise reduction and rain protection. This makes the BEAR able to operate in all kinds of environmental extremes.

Once the sonic boom data are collected, the RAM modules are transferred to the DRU for downloading the data. The Z-100 initiates its communications program (COMM) to accept this data from the DRU. These data are stored as two large raw data files (ABEARDAT.-B- & BBEARDAT.-B-) inside the Z-100. This file contains the BEAR setup parameters, boom data, captured data and parameter changes all separated by a series of three "barker codes" (hexidecimal values of 90 EB). The Z-100's process program then reads this file and breaks it up into individual files on each event that contain the data, plus all the BEAR parameter sets at the time that data were taken. Each file is given a specific file name corresponding to the date, time and location of its occurrence according to the following scheme. (i.e. PSSHHmmI.MDD, where P indicates a processed event, SS = site number, HHmm = local time in hours and minutes, I = incrementer (A..Z) to differentiate between events that occurred in the same minute at the same location, MDD = month and day). For this test the serial number of each BEAR was input as the site number since all were located at the same location. These files are stored on a floppy disk in a binary format and can be graphically displayed on the Z 100 by invoking the VIEW command.

Each BEAR system was carefully calibrated in the Laboratory to balance each microphone to the BEAR A to D circuitry and adjusted to a precision voltage source to verify the absolute levels recorded. In addition, each BEAR was checked with a 124 dB 250 Hz piston-phone calibrator before and after each aircraft flight. This calibration signal was saved by each BEAR to form a permanent record of the stability of each system. This procedure is used to verify an end to end acoustic calibration traceable to the National Bureau of Standards. The BEAR systems are explained in greater detail in a companion AAMRL report.

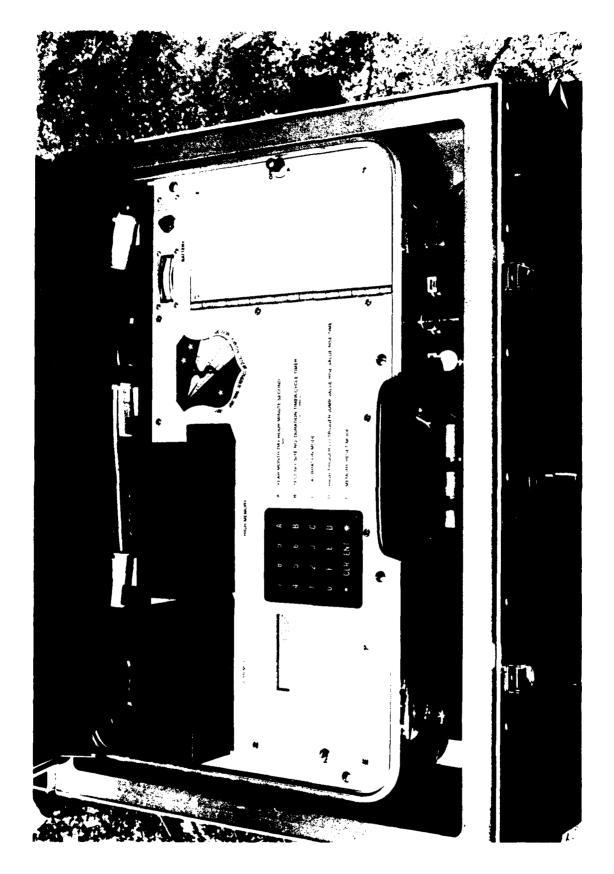


Figure 1. Boom Event Analyzer Recorder (BEAR)

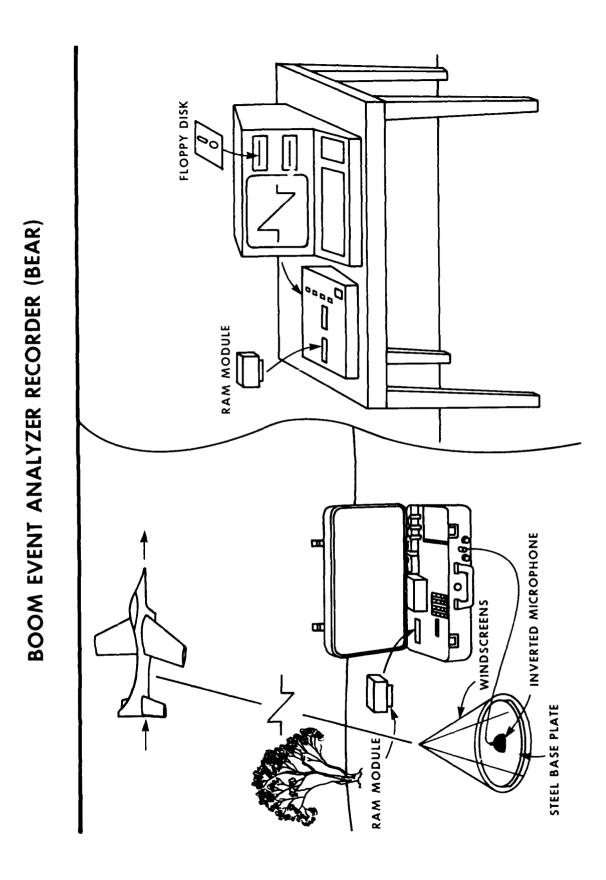


Figure 2. BEAR Field/Lab Setup

NASA Analog Sonic Boom Measurement System

The NASA analog sonic boom measurement system has been used in previous aircraft, Apollo, Skylab, and space shuttle sonic boom measurement programs and consists of pressure transducer, Dynagage (oscillator-detector circuit), instrumentation amplifier, FM magnetic tape recorder, and satellite time code receiver. The pressure transducer is a commercially available condenser microphone considered to have a flat frequency response for the lower frequencies required for sonic boom measurement. The microphone used for sonic boom measurements and in conjunction with the model DG-605 Dynagage system has a high frequency response essentially flat to 10K Hz, with the low end frequency response averaging approximately -5 dB at .01 Hz. Basically, the microphone has a small capillary hole through the housing which allows some air flow so that the static pressure within the capsule always equals the ambient atmospheric pressure. Thus, the acoustic loading is the same on both sides of the diaphram even at frequencies well below 20 Hz. This technique will allow adequate provisions for system balancing and tuning in addition to coping with various ranges of temperature and atmospheric pressure changes that could occur during diversified field measurement operations.

The Dynagage consists of a radio frequency oscillator coupled to a diode detector circuit whereby small changes in capacity of the pressure transducer will produce relatively large changes in the diode detector. The output of the detector is therefore proportional to the pressure applied to the transducer diaphram. The Dynagage output is fed into an instrumentation amplifier which provides a gain of 0 to 60 dB in steps of 2 dB with a flat frequency response of D.C. to 20 KHz.

The measurement system used frequency modulated magnetic tape recorders operating at 30 ips in the intermediate band with a frequency response of D.C. to 20 KHz. Electrical power was furnished by portable gasoline generators. This instrumentation was mounted in a covered truck 1000 ft from the 4 x 4 ft ground board.

All microphones were covered with wind screens consisting of three layers of cheesecloth to minimize effects of surface winds on the microphone readings and also to provide shade from the sun and protection from blowing sand particles. The output of the microphones were routed through the instrumentation amplifiers thus allowing for the setting of a range of overpressure levels (a precaution necessary to allow for errors in the predictive method or anomalous overpressures caused by unusual atmospheric or focusing conditions). Twelve channels of overpressure data were recorded along with time code signal, and voice annotation. All systems were "warmed up" for 2 hours prior to each test. All tape recorder data channels were calibrated using a precision voltage source to verify center frequency stability, all microphones were calibrated at both "pre" and "post" flight conditions using a fixed frequency sound pressure level calibrator to verify an end-to-end acoustic calibration Traceable to the National Bureau of Standards. A block diagram and photograph of a typical data acquisition system is shown in figures 3 and 4 respectively.

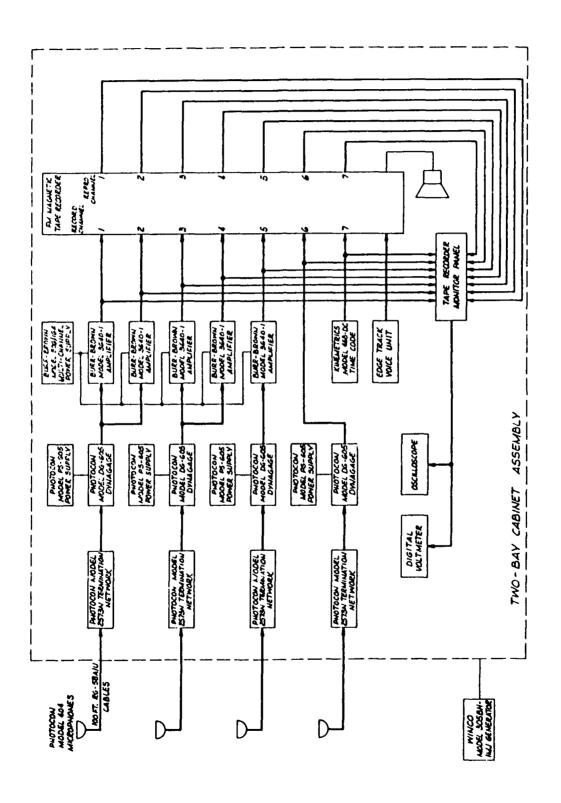
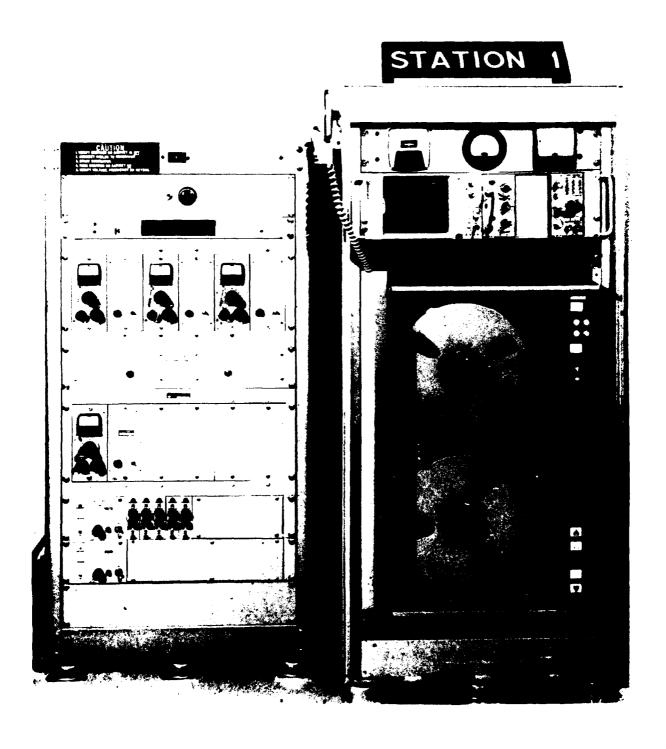


Figure 3. Block Diagram of NASA Analog Sonic Boom Measurement System



'Figure 4. NASA Analog Sonic Boom Measurement System

Comparison Test at Edwards Air Force Base

Sonic boom measurements were conducted on 16 - 18 Sep 86 at Edwards AFB CA under the Alpha Supersonic Corridor. Twelve BEAR units and the NASA analog system with 12 microphones were used for this test. The first day was used to compare outputs in the normal NASA microphone configuration (flush mounted) to give a comparison of similar signature outputs of both systems. (Figure 5) For this test all the BEARs and four NASA microphones were mounted in a 1 foot square phenolic holder which was mounted to a 4 x 4 sheet of 3/4 inch plywood. (Figure 6) A hole was dug and the plywood placed over the hole allowing all the microphones to be be flush mounted within a one square foot area. In addition to the microphones to be used for the comparison test, NASA microphones were placed on a 30 ft mast to collect data for full field comparisons. (Figure 7) With all the equipment set up and verified the F-4 aircraft conducted the supersonic overpasses as per Table 1. Each evening these data were collected and downloaded to be prepared for the next days test.

The second day was used to check the proposed AAMRL configuration of an inverted microphone and compare the results with the flush mounted approach. For this test all the NASA microphones remained the same as the first day's test. The BEAR microphones were rearranged as per Figure 8. The BEAR systems 1 through 3 were left flush mounted. The AAMRL Inverted Microphone Mount (Figure 9) was used for BEAR systems 8 through 13. The angle bracket (Figure 10) was used on BEAR systems 4 through 7 to test the effect of the boom shock wave striking the microphone diaphragm at various angles.

Figure 11 shows this 17 Sep 86 setup. The F-4 and F-111 aircraft flew the supersonic overpasses as per Table 2.

The third day was not originally scheduled for the comparison test but presented an opportunity to collect several F-4 supersonic overpasses at a different location. This test demonstrated the BEAR's versatility and mobility. We were able to set up 5 BEARs at a completely new location within 30 minutes of the overflights. All five of these BEARs were set up using the AAMRL Inverted Microphone Mount. The F-4 aircraft flew the supersonic overpasses as per Table 3.

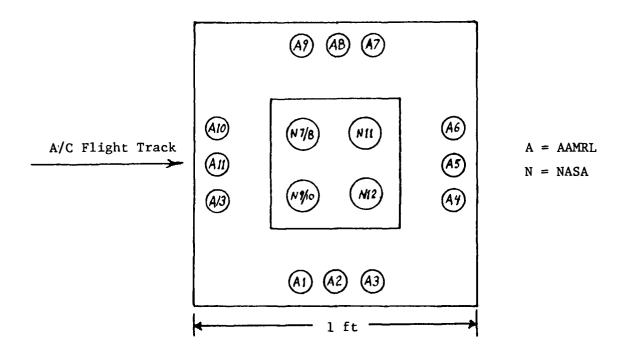


Figure 5. Microphone Setup for 16 Sep 86



Figure 6. Microphone Flush Mount Bracket

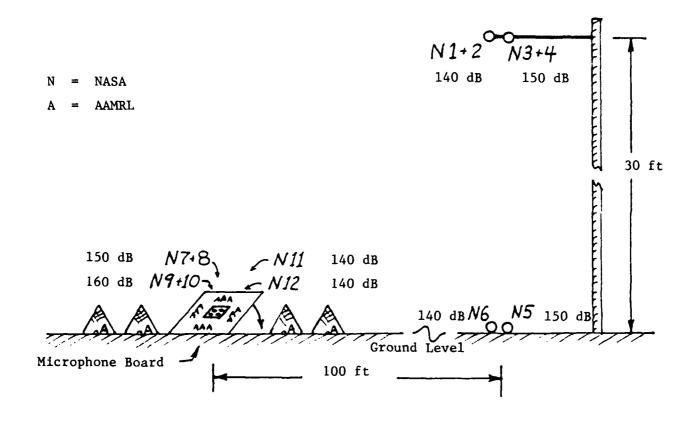


Figure 7. NASA Analog Tape Recorder Channel Assignment

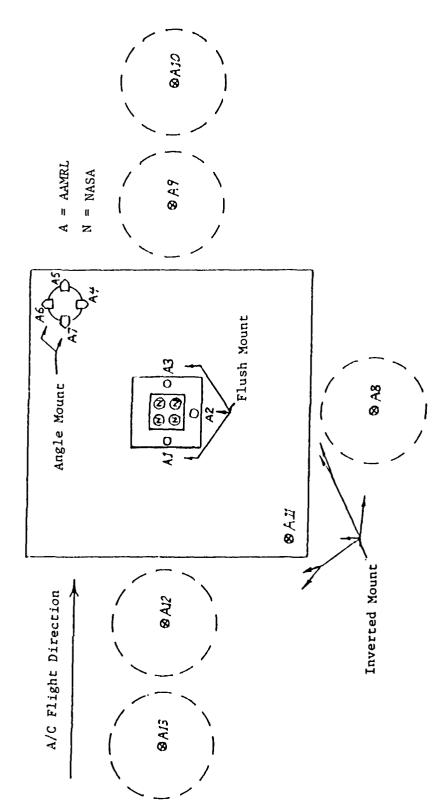


Figure 8. Microphone Setup for 17 Sep 86

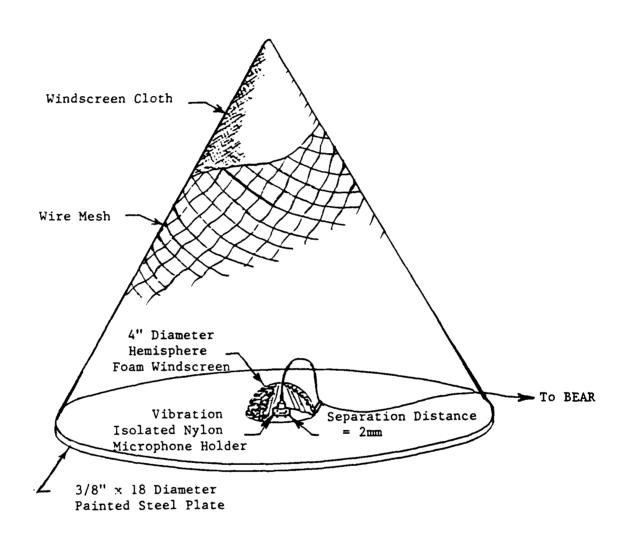


Figure 9. AAMRL Inverted Microphone Mount



Figure 10. Microphone Angle Bracket

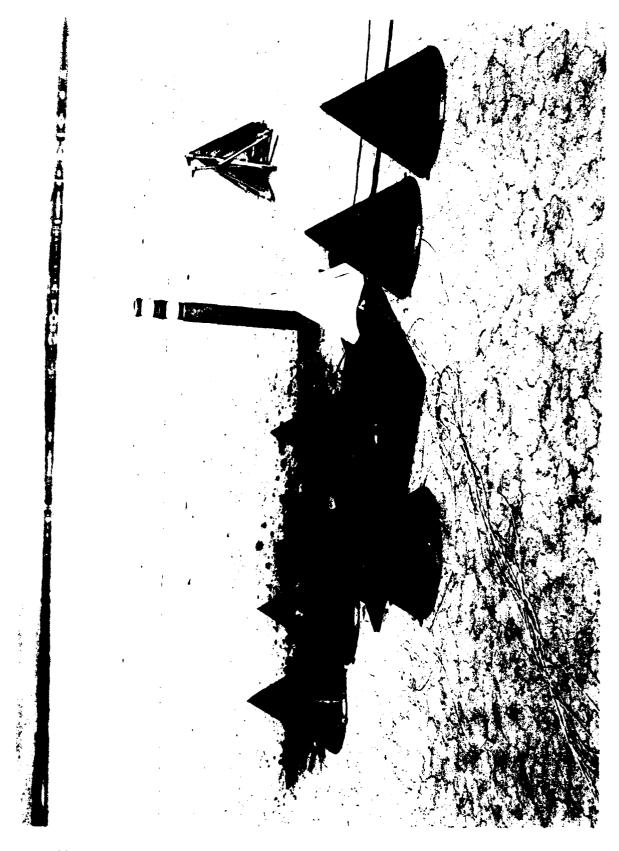


Figure 11. 17 Sep 86 Sonic Boom Test at Edwards AFB

TABLE 1

16 Sep 86 Boom Overflight Description

Air Force - NASA BEAR Calibration Test at Edwards AFB

| | | | | | ALT | | В | DOM |
|---|---------|----------------|-----|-------------|--------|--------------|---------|----------|
| | | NASA | | | (AGL) | Track Offset | Time | Time |
| • | EVENT # | MISSION # | A/C | Mach Number | (feet) | (feet) | (local) | (zulu) |
| | 2 | 19K-2 | F-4 | 1.2 | 18,900 | 0 | 8:16 | 15:16:38 |
| | 3 | 5K-1 | F-4 | 1.15 | 6,000 | 0 | 8:20 | 15:20:08 |
| | 4 | 35K-1 | F-4 | 1.45 | 35,000 | 60600 | 8:33 | 15:33:04 |
| | 5 | 19K-1 | F-4 | 1.2 | 20,700 | 0 | 16:17 | 23:17:47 |
| | 6 | 5K - 2 | F-4 | 1.15 | 5,500 | 0 | 16:22 | 23:22:22 |
| | 7 | 35K - 2 | F-4 | 1.45 | 35,100 | 60600 | 16:31 | 23:31:45 |
| | 8 | 5K-3 | F-4 | 1.15 | 5,200 | 0 | 16:35 | 23:35:18 |

TABLE 2

17 Sep 86 Boom Overflight Description

Air Force - NASA BEAR Calibration Test at Edwards AFB

| | | | | ALT | | B00I | 4 |
|---------|----------------|--------|------------|----------|------------|---------|----------|
| | NASA | | | (AGL) Tr | ack Offset | Time | Time |
| Event # | MISSION # | A/C M | ach Number | (feet) | (feet) | (local) | (zulu) |
| 1 | 19K - 4 | F-4 | 1.2 | 19,000 | 0 | 14:11 | 21:11:59 |
| 2 | 35K-3 | F-4 | 1.42 | 34,900 | 60600 | 14:20 | 21:20:54 |
| 3 | 35K-4 | F-4 | 1.35 | 35,200 | 60600 | 14:26 | 21:26:16 |
| 4 | 5K-4 | F-4 | 1.13 | 5,700 | 0 | 14:31 | 21:31:08 |
| 1 | 1K-1 | F-111A | 1.03 | 1,200 | 0 | 15:02 | 22:02:33 |
| 2 | 1K-2 | F-111A | 1.04 | 1,200 | 0 | 15:07 | 22:07:49 |

TABLE 3

18 Sep 86 Boom Overflight Description

Air Force - NASA BEAR Calibration Test at Edwards AFB

| | | | ALT | | | B00M | | |
|---------|----------------|-----|-------------|------------|----------|---------|--------|--|
| | NASA | | | (AGL) Trac | k Offset | Time | Time | |
| EVENT # | MISSION | A/C | Mach Number | (feet) (| feet) | (local) | (zulu) | |
| 1 | 35K - 5 | F-4 | 1.22 | 34,200 | 0 | 9:09 | 16:09 | |
| 2 | 35K-6 | F-4 | 1.28 | 32,900 | 0 | 9:16 | 16:16 | |
| 3 | 35K-7 | F-4 | 1.14 | 34,700 | 0 | No Boom | | |
| 4 | 35K - 8 | F-4 | 1.35 | 34,100 | 0 | 9:32 | 16:32 | |

RESULTS

SIGNATURE COMPARISONS

The aircraft overflights were flown to provide boom overpressures from less than 1 PSF to over 20 PSF to check the BEAR over the range of booms generated by typical Air Force operations. When comparing the NASA signatures to the AAMRL BEAR signatures it must be remembered there is a difference in low frequency cut-off between the two different microphone systems. The NASA microphones have a low frequency response down to .01 Hz. AAMRL designed the analog front end of the BEAR systems to a .5 Hz requirement. This low frequency cut-off difference will cause the AAMRL signatures to vary slightly from the NASA measurements. An idealized N-wave with duration typical of those collected (less than 200 milliseconds) passed through a .5 Hz high pass filter vs a perfect DC high pass filter will introduce an error of less than ldB in the peak pressure value and less than .5 dB in the flat weighted sound exposure level (SEL). This was an acceptable compromise for the BEAR system design.

Flush Mount Microphone

Figures 12 through 15 are the pressure-time history comparisons of the AAMRL BEARs to the NASA boom measurement systems, both using flush mounted microphones. Each of these plots represent all the data that were recorded for a particular overflight. These figures show the variability of the boom signatures as measured within the 1 square foot area containing all the microphones. Figure 16 shows a similar pressure-time history comparison but with a very pronounced oscillation in several of the BEAR system signatures. We believe that this is due to a resonance of the one square foot plate on which the BEAR microphone is mounted being forced by the sonic boom. This boom occurred at 8:19 on 16 Sep 86. BEAR microphones 4 & 5 were perpendicular to the boom (see figure 5). Microphone 5 was in the center where you would expect the most oscillation, and microphone 4 was closer to where the holder was fastened to the plywood. In the individual signatures (see Appendix) we see that the oscillation starts at microphone 4, builds to a maximum at microphone 5, with no detectable oscillation on the other BEAR microphones. Except for this oscillation, all the other BEAR collected signatures show great agreement with the signatures collected by the NASA systems.

Inverted to Flush Mount Comparisons

Figures 17, 18 and 19 are comparisons of three BEAR-collected pressure-time histories using the flush mounted BEAR microphones and the AAMRL inverted microphone mount (see Figure 9). These signatures and the following comparisons are representative of the BEAR outputs with each comparison showing all the data that were collected on each boom (several BEAR signatures were lost due to voltage drift of the microphone caused by thermal overload that was not accounted for). NOTE: This problem was corrected in the BEARs after completion of this test. Except for the normal differences between each microphone, these data show great agreement between these two mount configurations over the complete BEAR pressure range.

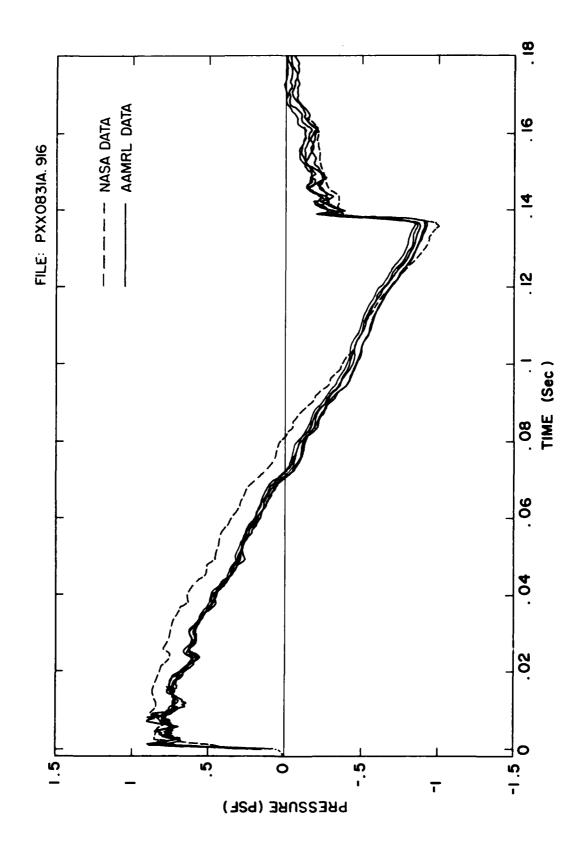


Figure 12. 1 PSF Boom Signature Comparison

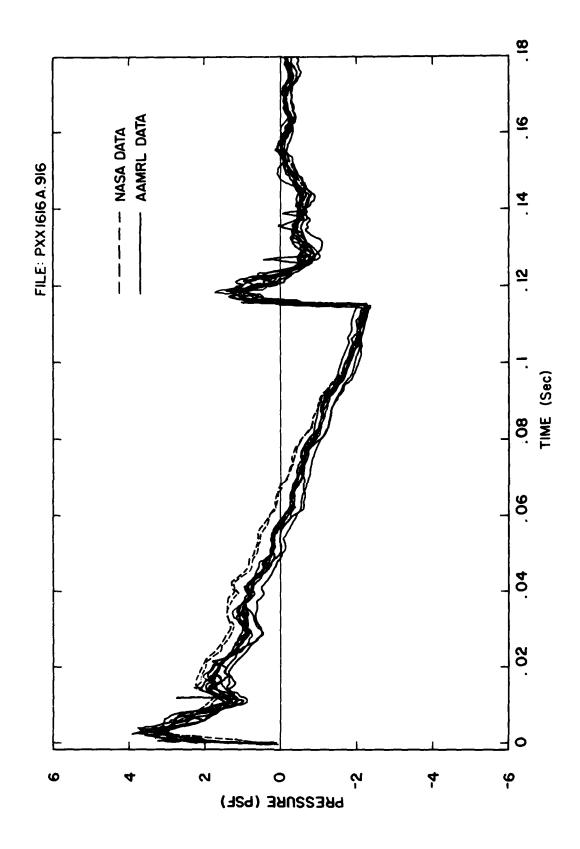


Figure 13. 4 PSF Boom Signature Comparison

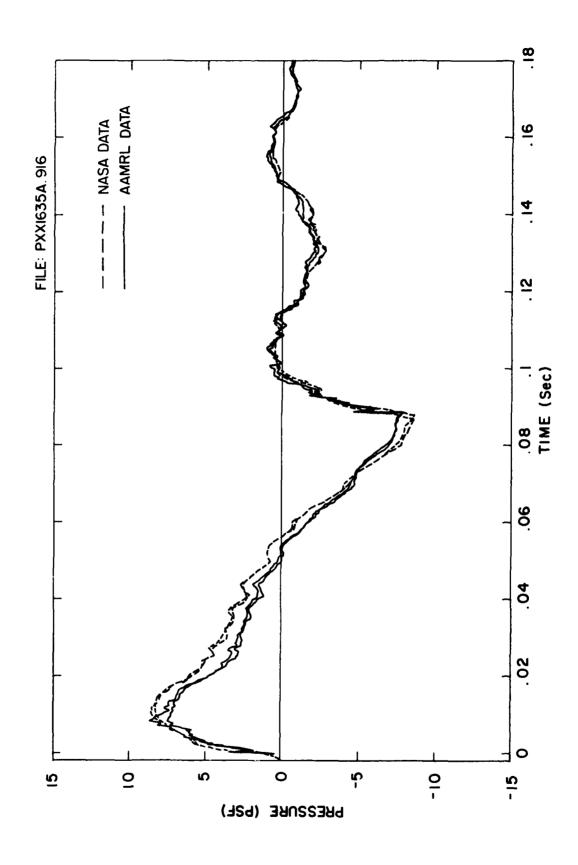


Figure 14. 9 PSF Boom Signature Comparison

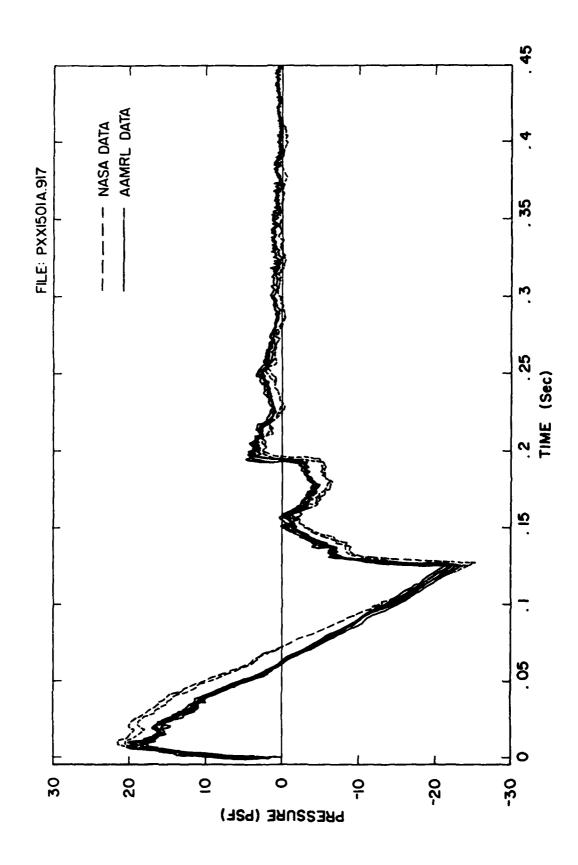


Figure 15. 20 PSF Boom Signature Comparison

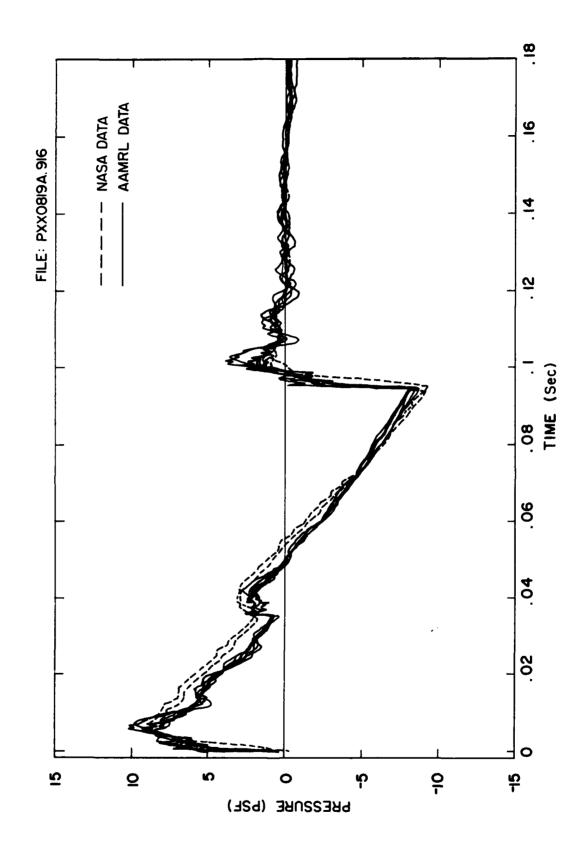


Figure 16. 10 PSF Boom with Resonance from Board Mount

Angle Mount Comparisons

Figures 20, 21 and 22 are comparisons of three BEAR collected pressure-time histories using the flush mounted microphone and the angle mounted microphones (see Figure 10). Again, we see great agreement between these mount configurations. Since the angled microphones were mounted on an angled wire mount, they were also very susceptible to boom induced oscillation. This can also be seen on several of these boom comparisons and is not indicative of the BEAR performance.

Figures 23, 24 and 25 are comparisons of three BEAR collected pressuretime histories using the AAMRL inverted microphone mount and the angle mounted microphones. Again, we see great agreement between these mount configurations.

Table 4 summarizes these differences for the three mount configurations across these three events. The positive peak pressure values (in dB and PSF), as well as the time integrated values of non-weighted sound exposure level (FSEL), C-weighted sound exposure level (CSEL) and A-weighted sound exposure level (ASEL) are shown for all these events. Table 4 shows the FSEL and CSEL all agree within about .5 dB whereas the ASEL has variations of up to 3 dB for the same event.

The ASEL metric itself as applied to sonic booms causes large variations in the ASEL values. The major part of the energy of a sonic boom is at its fundamental frequency usually below 10 Hz. The A-weighting greatly reduces the contribution of the low frequencies making the higher frequencies dominate the ASEL Metric. These higher frequencies are more susceptible to local conditions from microphone to microphone contributing to the variation in the ASEL metric. Note that these variations in the ASEL are not due to mount configuration because some of the largest variations are between the same mount configuration.

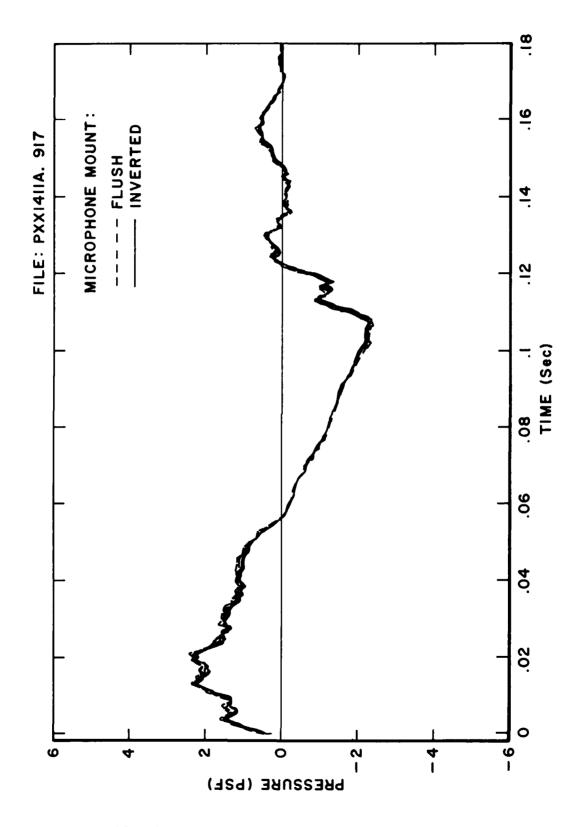


Figure 17. 2.5 PSF Inverted vs Flush Mount Comparison

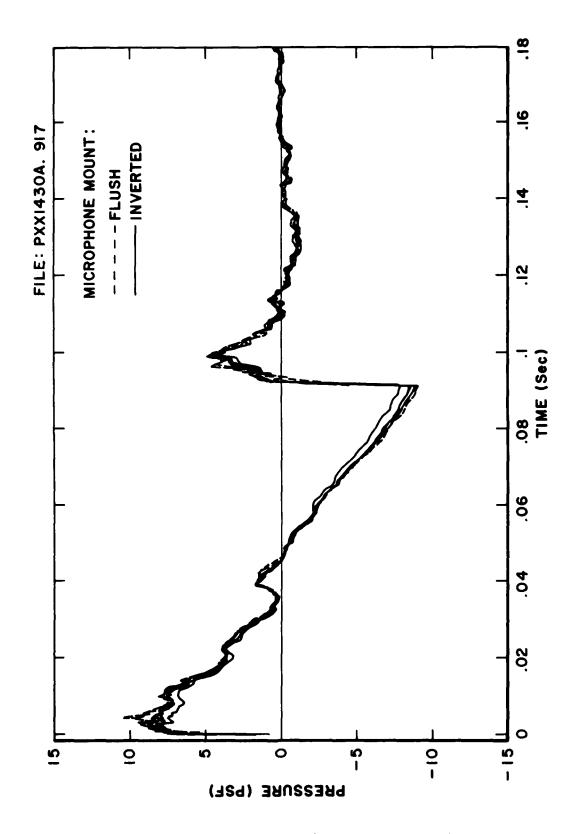


Figure 18. 10 PSF Inverted vs Flush Mount Comparison

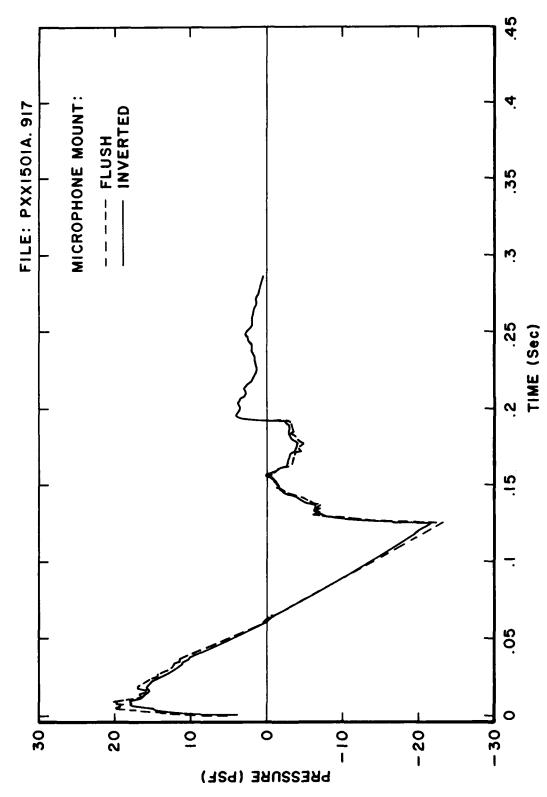


Figure 19. 20 PSF Inverted vs Flush Mount Comparison

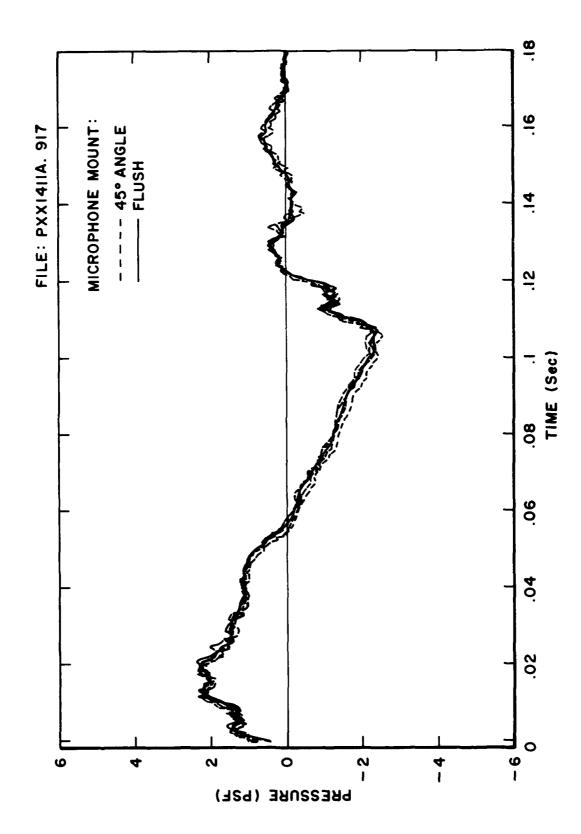


Figure 20. 2.5 PSF Angle vs Flush Mount Comparison

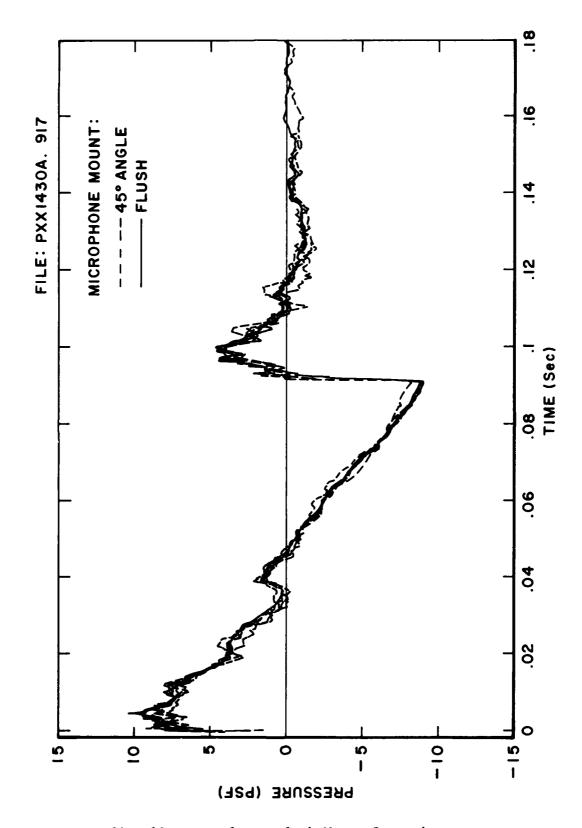


Figure 21. 10 PSF Angle vs Flush Mount Comparison

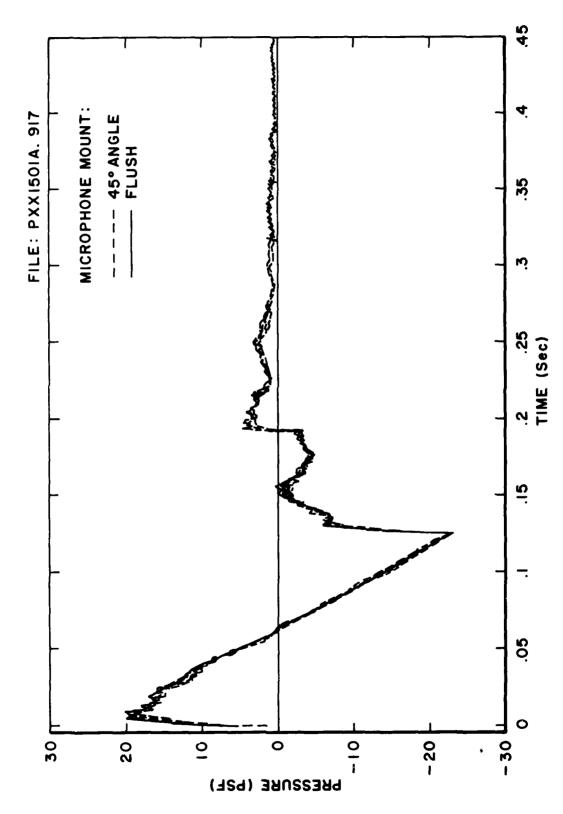


Figure 22. 20 PSF Angle vs Flush Mount Comparison

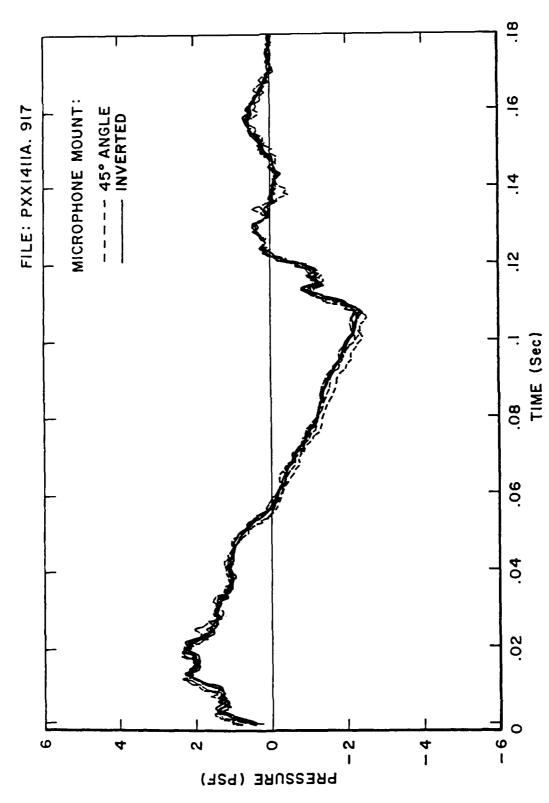


Figure 23. 2.5 PSF Angle vs AAMRL Inverted Mount Comparison

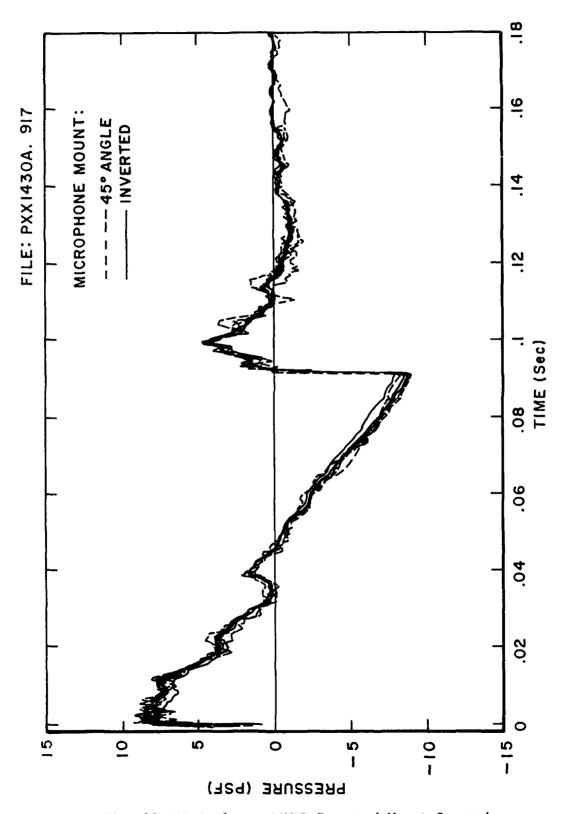


Figure 24. 10 PSF Angle vs AAMRL Inverted Mount Comparison

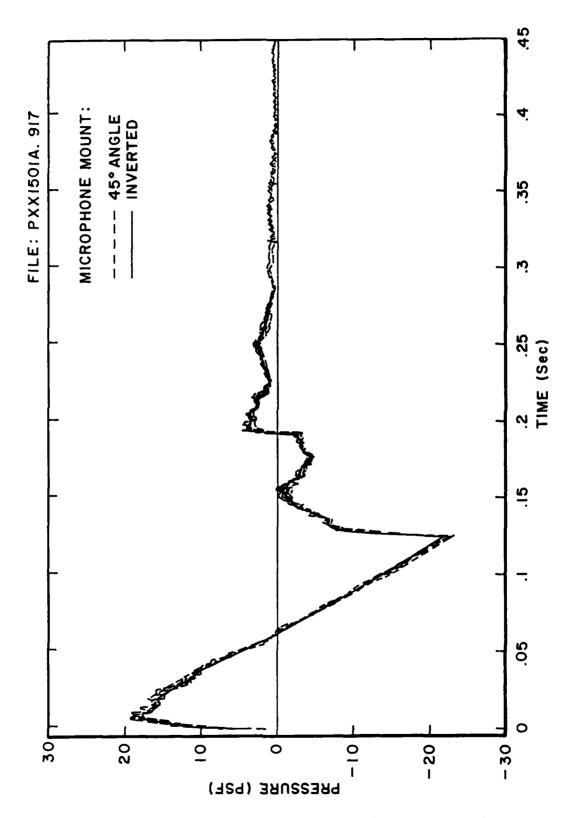


Figure 25. 20 PSF Angle vs AAMRL Inverted Mount Comparison

TABLE 4

Microphone Mount Comparisons

| ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |
|-----------------------|--|---|--|---|--|--|---|
| DATE | BEAR SN | CONFIGURATION | PK (dB) | PK (PSF) | ASEL | CSEL | FSEL |
| 17 SEP 86 14:11 pm | 1 3 4 5 6 7 8 9 | FLUSH MOUNT FLUSH MOUNT 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE BBE MOUNT BBE MOUNT BBE MOUNT | 135.0 135.6 135.4 135.3 135.4 135.3 134.7 135.2 135.0 | 2.3 2.5 2.5 2.4 2.5 2.4 2.3 2.4 2.3 | 89.8 89.6 90.2 | 109.2 108.8 | 121.3 121.9 121.6 |
| ***** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |
| DATE | BEAR SN | CONFIGURATION | PK (dB) | PK (PSF) | ASEL | CSEL | FSEL |
| 17 SEP 86 14:30 pm | 1 3 4 5 6 7 8 9 10 11 12 | FLUSH MOUNT FLUSH MOUNT 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE BBE MOUNT BBE MOUNT BBE MOUNT BBE MOUNT BBE MOUNT | 147.5 148.2 147.2 146.8 146.1 146.3 146.1 146.7 146.4 146.6 | 9.9 10.7 9.6 9.1 8.4 8.6 8.4 9.0 8.7 8.9 | 105.9 108.2 109.6 108.4 108.7 108.5 107.5 107.4 107.2 107.0 | 124.6 124.2 124.5 124.3 124.1 123.9 124.3 124.1 123.9 124.3 | 131.6 132.0 131.9 131.9 131.3 131.8 131.5 131.4 131.8 |
| ****** | ***** | ***** | ***** | ***** | ***** | ***** | ***** |
| DATE | BEAR SN | CONFIGURATION | PK (dB) | PK (PSF) | ASEL | CSEL | FSEL |
| 17 SEP 86 15:01 pm | 2 3 4 5 6 7 8 | FLUSH MOUNT FLUSH MOUNT 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE 45 DEG ANGLE BBE MOUNT | 154.1 153.9 153.5 153.8 153.6 153.3 152.7 | 21.1 20.7 19.7 20.4 20.0 19.3 18.0 | 110.3 108.7 109.8 108.8 110.5 110.1 107.5 | 127.7 128.0 127.9 | 141.5 141.5 141.4 141.8 141.6 141.4 140.9 |

FREQUENCY ANALYSIS COMPARISON

Both the AAMRL BEAR and the NASA analog system collected data were processed to obtain the one hertz band width sound exposure spectrum level plots. Flat Weighted Sound Exposure Levels (FSEL), A-weighted Sound Exposure Levels (ASEL) and the C-weighted Sound Exposure Levels (CSEL). The BEAR data were transferred to the AAMRL mainframe computer and processed through the AAMRL BOOMBEAR Program. The BOOMBEAR Program takes the BEAR pressure-time digitized waveform and transforms it into a pressure-frequency plot using the Fast Fourier Transform (FFT). Since the BEAR captures just the boom signature, typically around 200 milliseconds, the event was zero filled out to one second before inputting to the BOOMBEAR program. This zero filling technique adds a sound pressure value of zero to the event effectively adding no energy but allows direct comparison to the NASA data that always used one second of the analog recording that contained the sonic boom. The NASA data were first digitized at 8000 points per second and then run through the NASA SBFFT program; the NASA SBFFT Program also converts from the pressure-time plots to the pressure-frequency plots via the FFT algorithm. Since this one second contained background and electronic noise floor data of the NASA recording system, some of the NASA events show higher levels at the higher frequencies that are not dominated by the boom event.

Figures 26 through 30 are the frequency comparisons for several booms ranging from more than 20 PSF to less than 1 PSF. Figures 27 and 28 show the results of two similar runs (F-4 at 5000 ft altitude AGL) during morning and afternoon runs. Figure 27 from the morning run, had a fairly clean distinctive F-4 N-wave. Figure 28 from the afternoon run, had a slightly distorted (from the atmospheric disturbance) N-wave that shows up in the slightly distorted frequency plots.

Table 5 presents the single metric comparisons between the two systems. The comparisons are made with representative signatures from the BEAR and NASA systems. There is good agreement between these values for the two systems except for the A-weighted SEL's. (See Table 6) This is due to the high frequency components that are in the NASA data discussed above. This is not part of the sonic boom but is due to the limited dynamic range of the instrumentation that was used by NASA. The low frequency energy is heavily weighted and virtually ignored with the A-weighting. Therefore, the low-level higher-frequency data, including the electronic noise floor of the recording system, become important to the A-weighted metric but are not representative of the major energy of a typical sonic boom.

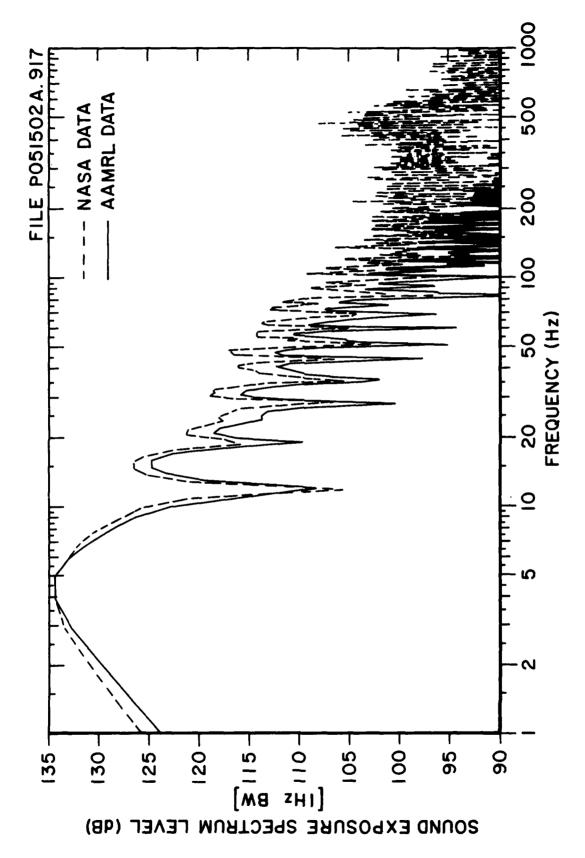


Figure 26. 20 PSF Boom Spectrum Comparison

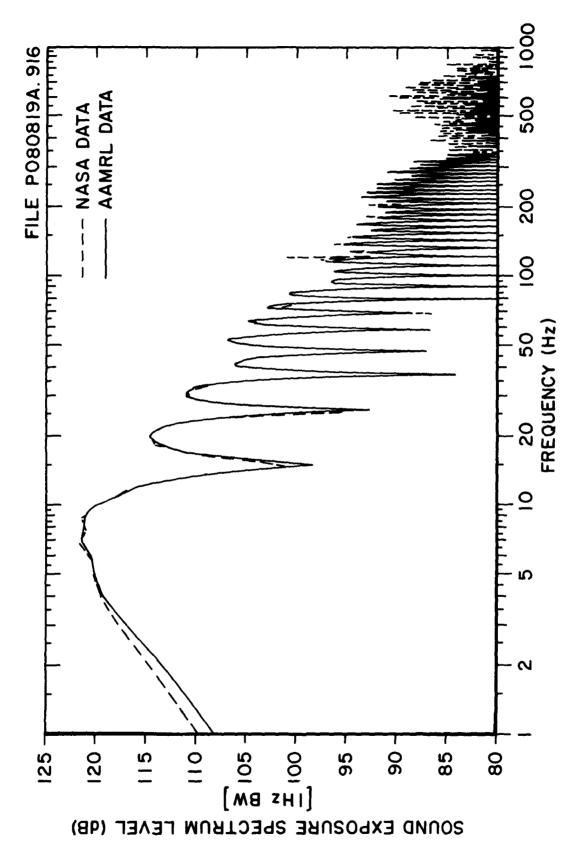


Figure 27. 8 PSF Clean Boom Spectrum Comparison

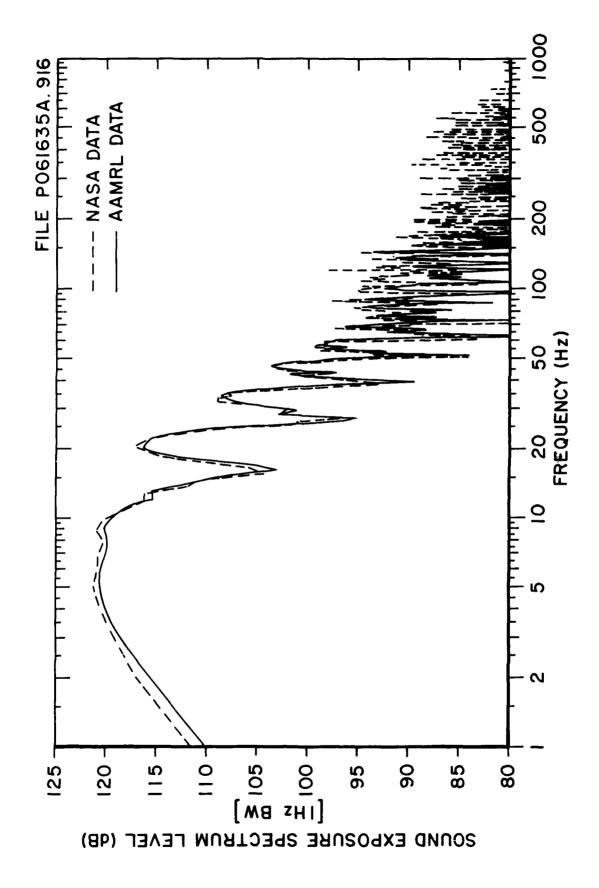


Figure 28. 8 PSF Distorted Boom Spectrum Comparison

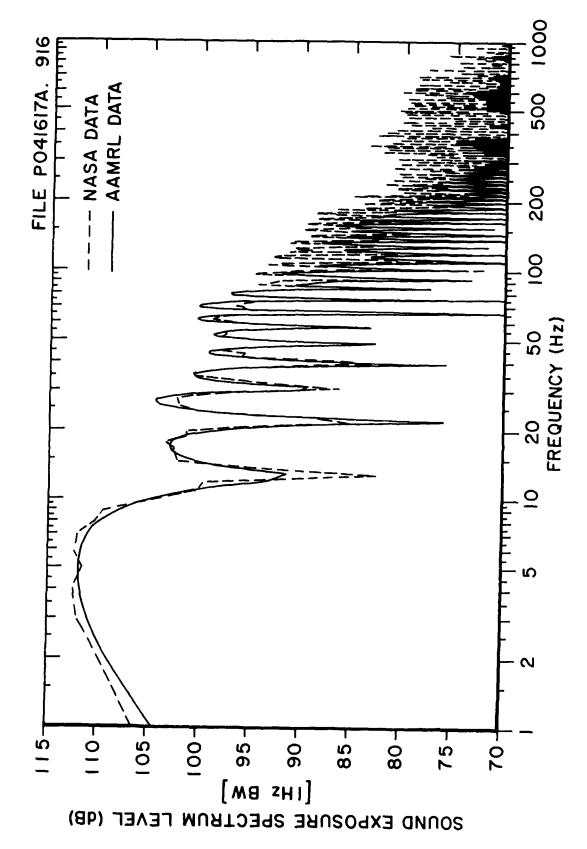


Figure 29. 3.6 PSF Boom Spectrum Comparison

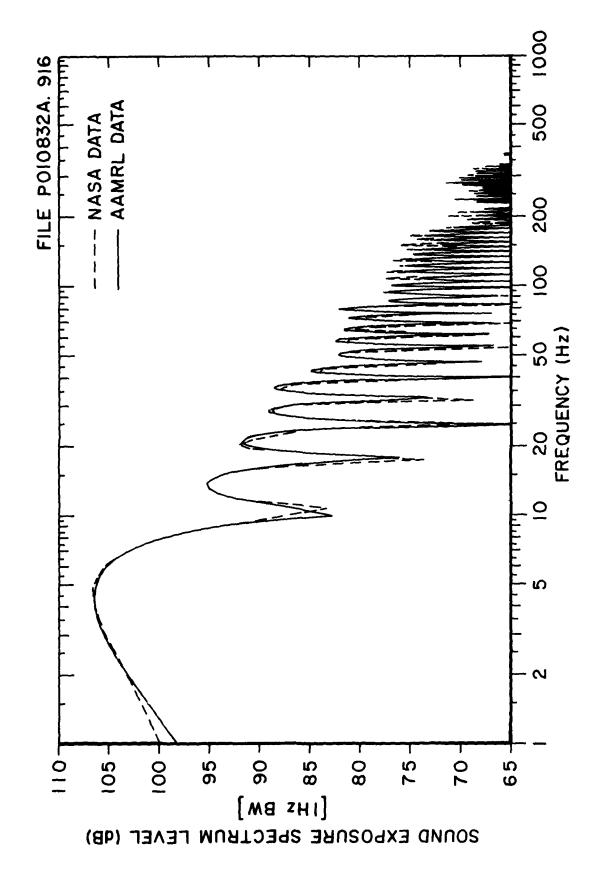


Figure 30. .9 PSF Boom Spectrum Comparison

TABLE 5

NASA to Air Force Single Metric System Comparisons

| NASA | | AAN | MRL SINGLE METRIC | E METRIC | | BEAR | NA | NASA SINGLE METRIC | METRIC | | NASA |
|---------------------------------------|------------------|-------|-------------------|-------------------|-------|--------|-------|--------------------|-------------|-------|--------|
| # # # # # # # # # # # # # # # # # # # | Time | Peak | FSEL | CSEL | ASEL | NUMBER | PEAK | FSEL | CSEL | ASEL | NUMBER |
| 35K-1 | 8:32 16Sep86 | 126.7 | 114.0 | 100.9 | 84.7 | 1001 | 127.4 | 114.2 | 100.7 | 87.8 | CH-7 |
| 19K-3 | 16:17 16Sep86 | 139.3 | 121.8 | 121.8 114.0 | 97.5 | 1003 | 139.6 | 122.2 | 114.5 | 102.6 | 6-H) |
| 5K-1 | 8:19 16Sep86 | 146.5 | 131.4 | 122.6 | 106.1 | 1010 | 146.5 | 131.4 | 122.6 | 111.2 | CH-10 |
| 5K-3 | 16:35 16Sep86 | 146.5 | 131.2 | 131.2 121.2 | 101.6 | 1004 | 146.4 | 131.7 | 121.5 | 107.7 | CH-10 |
| 1K-1 | 15:01 17Sep86 | 153.9 | 141.5 | 141.5 127.9 108.7 | 108.7 | 1003 | 154.1 | 141.8 | 141.8 128.3 | 116.3 | 6-H3 |

TABLE 6

NASA to Air Force Single Metric Systems Differences

| NASA Flight# | Time | Peak* | FSEL* | CSEL* | ASEL* | BEAR System Number | NASA System Number |
|-----------------|------------------|-------|-------|-------|-------|-----------------------|-----------------------|
| 35K-1 | 8:32 16Sep86 | 0.7 | 0.2 | 0.2 | 3.1 | 1001 | CH-7 |
| 19K-3 | 16:17 16Sep86 | 0.3 | 0.4 | 0.5 | 5.1 | 1003 | CH-9 |
| 5K-1 | 8:19 16Sep86 | 0.0 | 0.0 | 0.0 | 5.1 | 1010 | CH-10 |
| 5K-3 | 16:35 16Sep86 | -0.1 | 0.5 | 0.3 | 6.1 | 1004 | CH-10 |
| 1K-1 | 15:01 17Sep86 | 0.2 | 0.3 | 0.4 | 7.6 | 1003 | CH-9 |

* Values are NASA system values minus AAMRL BEAR values.

OTHER FACTORS

Clipped Signal

The last run of the F-111 aircraft on 17 Sep 86 created a boom of approximately 36 PSF overpressure. Since the BEAR's range was designed for 23.4 PSF maximum, this run demonstrated the operation of the BEAR in an overload condition. Since the BEAR is a digital system, when it is overloaded the signal is just clipped but not distorted unless the capacity of the microphone is exceeded (at 185 dB). The BEAR software still evaluates this event as a boom and captures it. Figure 31 shows this 36 PSF boom captured by the BEAR system and a NASA system. As can be seen, this clipped boom could be estimated fairly easily by extending the major slope of the N-wave. This would allow a person to recreate, with a reduced degree accuracy, a boom that was beyond the range of the BEAR's design.

Echos and Secondary Booms

Quite frequently when sonic booms occur, secondary booms occur from the same flight. These can be caused by the boom echoing off a nearby surface or the boom arriving from a slightly different ray path. If the separation of these booms is less than the event separation timer (timer 2) set value, the BEAR will simply capture both of these events on a single file. Figure 32 shows an example of how the BEAR captured this kind of secondary boom event. If the secondary boom were to occur later than what is set by timer 2, the BEAR would evaluate it as a separate boom event and store it in its own file. This allows the BEAR to capture any combination of booms occurring within the same time frame.

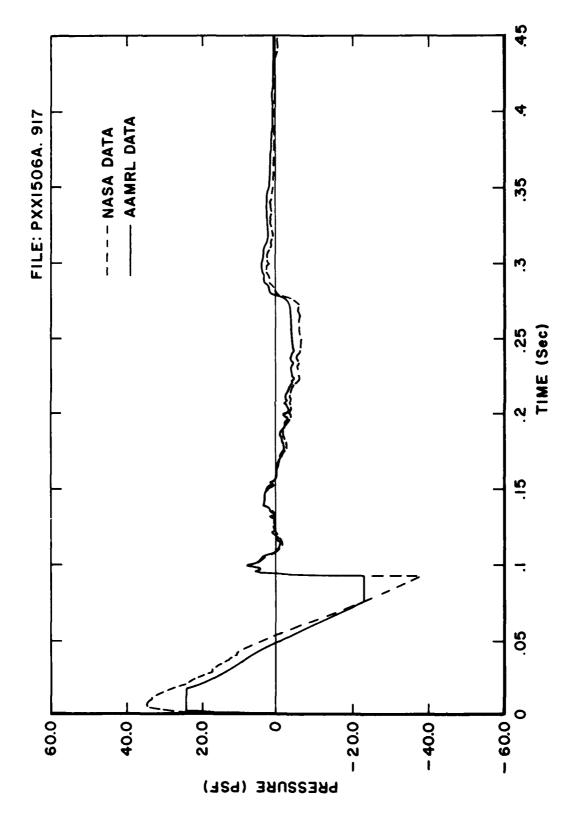


Figure 31. 36 PSF Clipped BEAR Signature

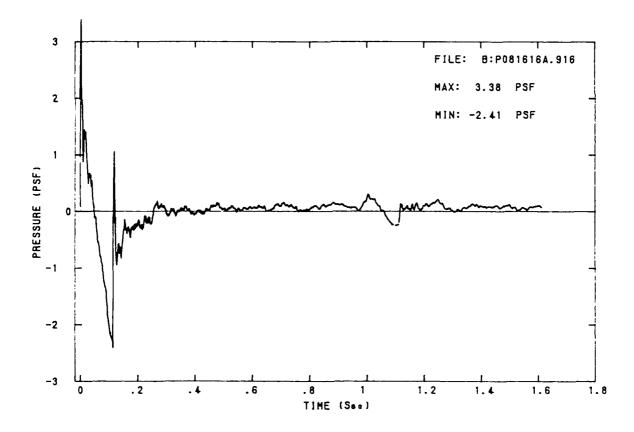


Figure 32. Secondary Boom

SUMMARY

This test demonstrated that the AAMRL BEAR systems are functionally equivalent to the NASA analog systems for capturing sonic boom waveforms. Typically the duration of sonic booms from supersonic military aircraft is around 200 milliseconds. The BEAR low-frequency cutoff of .5 Hz will introduce less than .5 dB error in the FSEL value at these durations. If the BEAR systems were to be used to collect boom waveforms greater than 500 milliseconds, the microphone and the interface amplifiers to the BEAR'S A/D converter should be changed to a lower low-frequency cutoff specification. This is fairly easy to do given the modular design of the BEAR system. This test also demonstrated that the proposed AAMRL inverted microphone mount is functionally equivalent to a flush mounted microphone for capture of sonic booms and can be used for future boom studies.

Several findings from these tests led to improvements in the BEAR's operation. Since the PCB microphones used with the BEAR can handle up to 185 dB and we don't need levels down to 65 dB, the BEAR operating range was shifted upwards by 10 dB. The BEARs now cover the range from 75 dB to 165 dB allowing capture of a boom up to 76.4 PSF without clipping. The non-boom rejection routines were improved to better compensate for the wind and thermal drift problems. Functionally the improvements do not affect the way the BEAR handles the incoming signal but only how it is interpreted once it comes through the A to D converter. Therefore, these changes will not affect these comparison results.

These BEARS were used in August 1987 to collect over 500 signatures from USAF and USN supersonic aircraft with greater than a 99% success rate in capturing the boom signatures. These data are presented in a companion report.

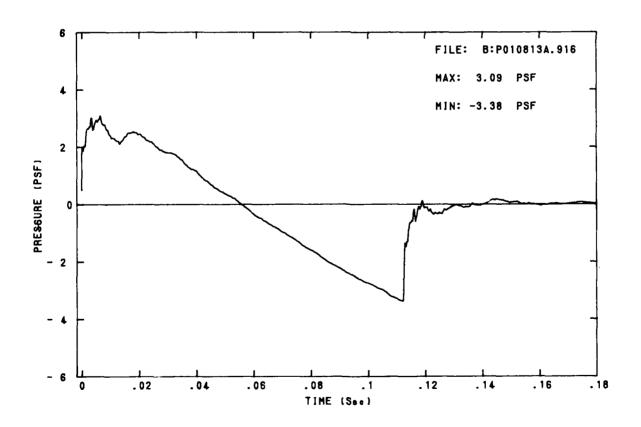
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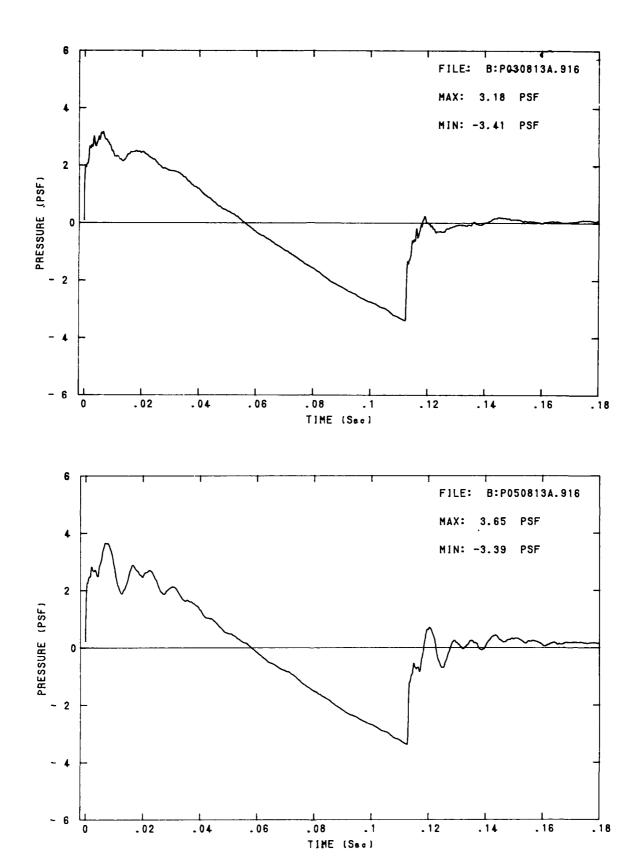
- Lee, Robert A.; Crabill, Monty; Palmer Barbara; Mazurek, Douglas, Ovenshire, David; Nuse, Kevin; Air Force Boom Event Analyzer Recorder (BEAR): System Description, AAMRL-TR-88-039, (in publication process).
- 2. Galloway, William, BBN Technical Memorandum to AAMRL, 6 July 1984
- 3. Lee, Robert A., AAMRL-TR-88-039, Sonic Booms Produced by USAF and USN Aircraft: Measured Data (in publication process).

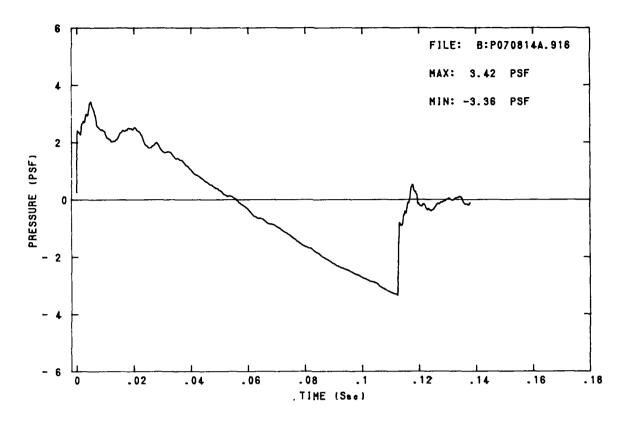
APPENDIX A

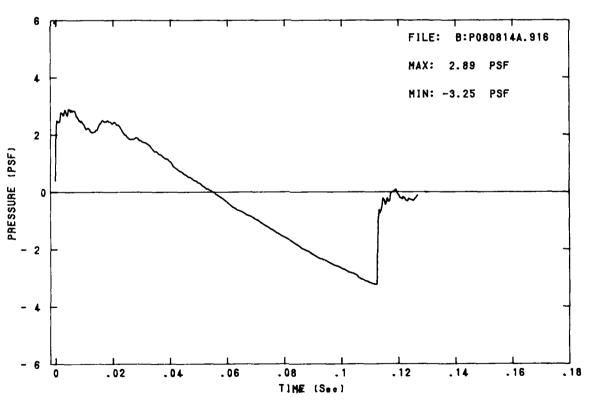
BOOM SIGNATURES

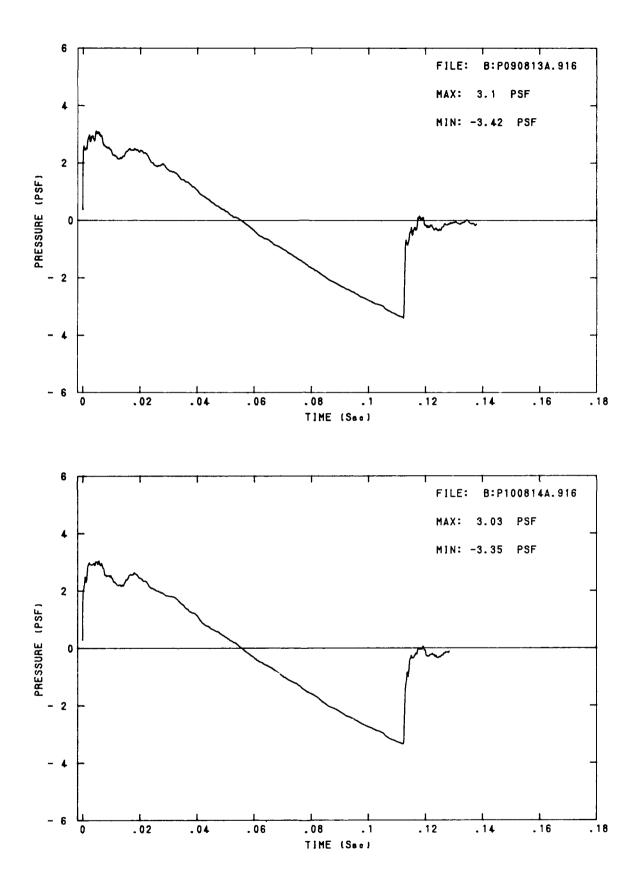
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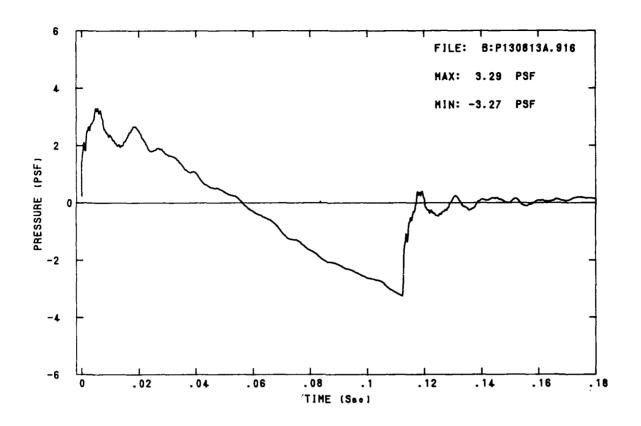


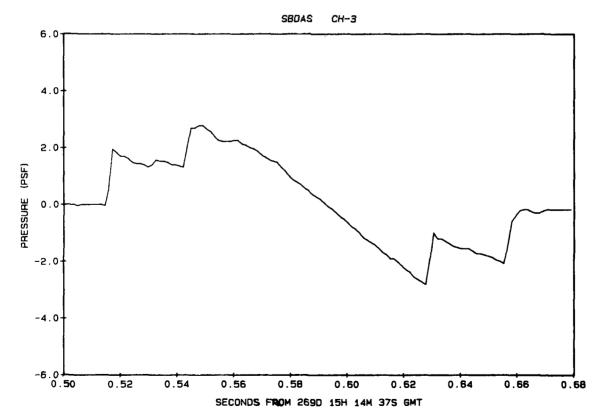


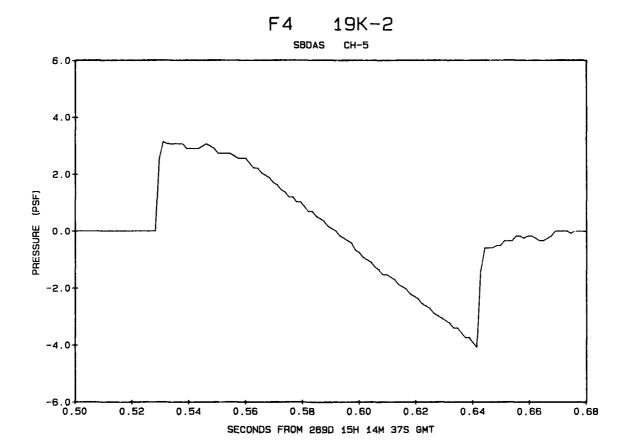


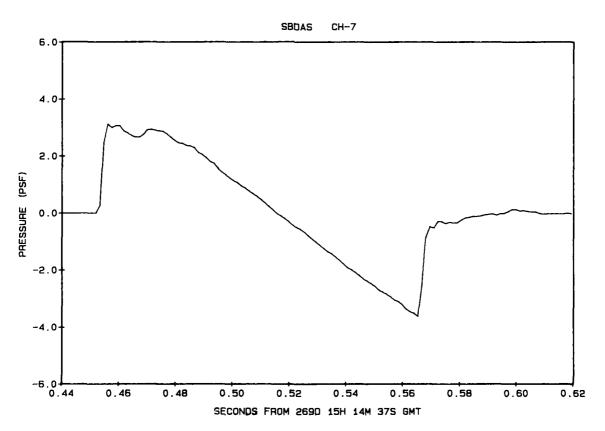


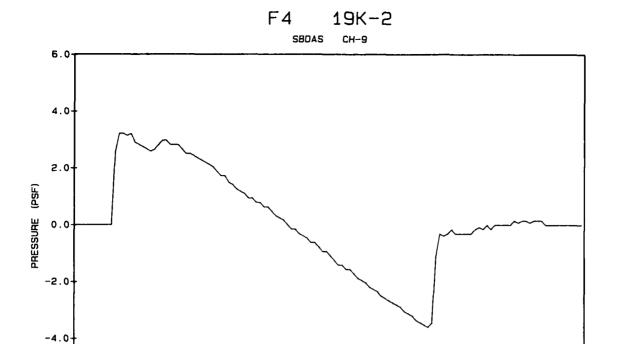












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0.60

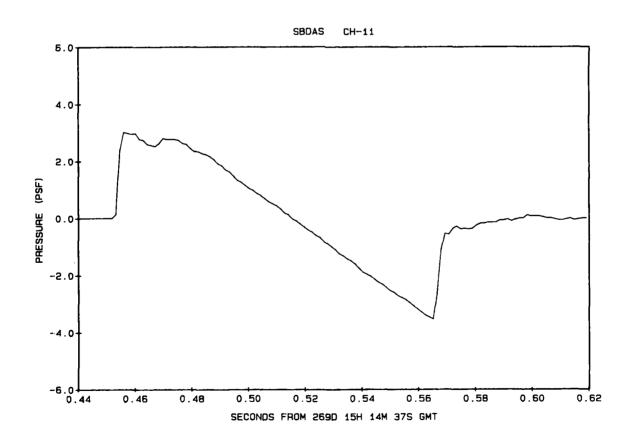
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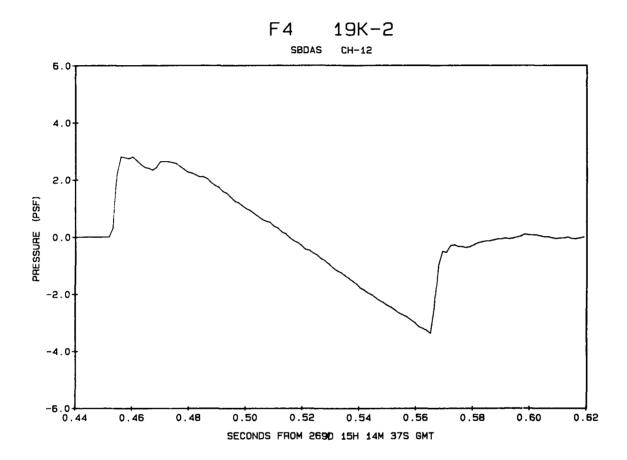
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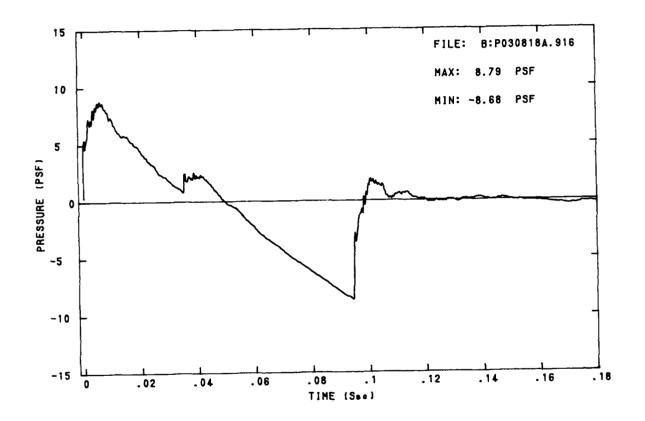
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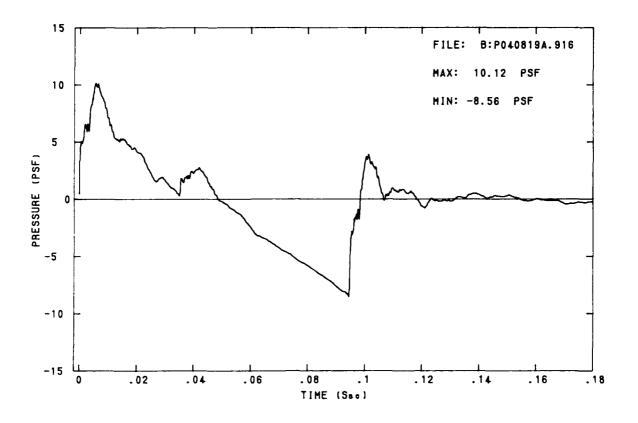
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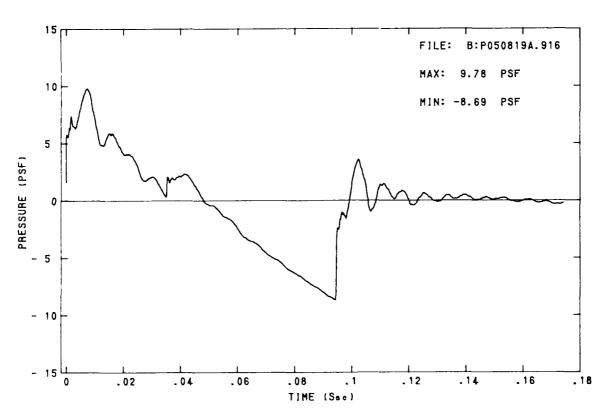


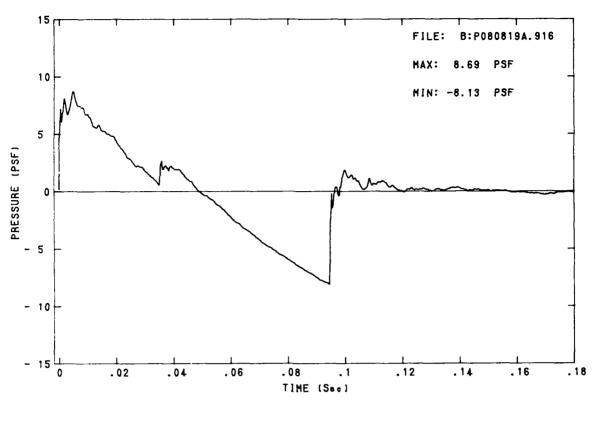


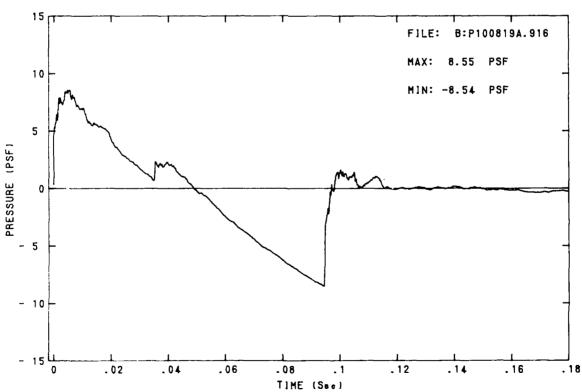
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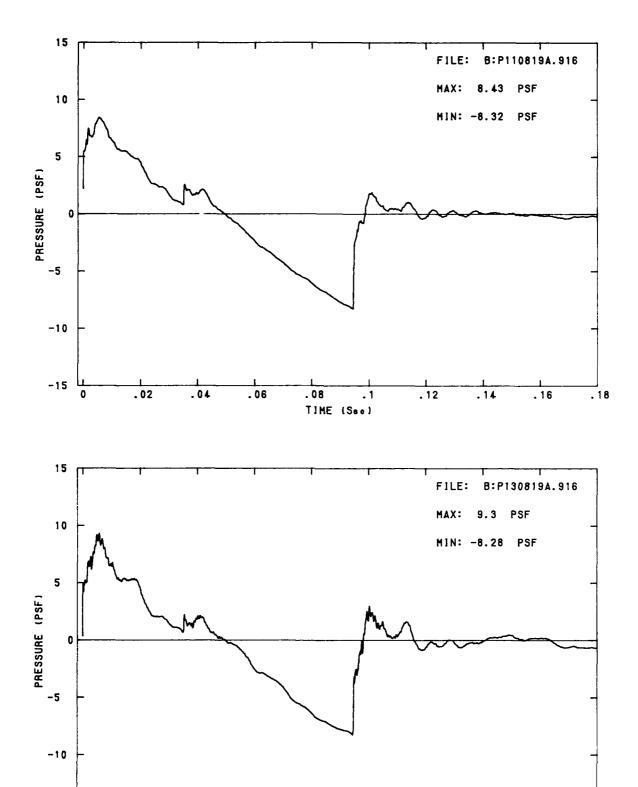












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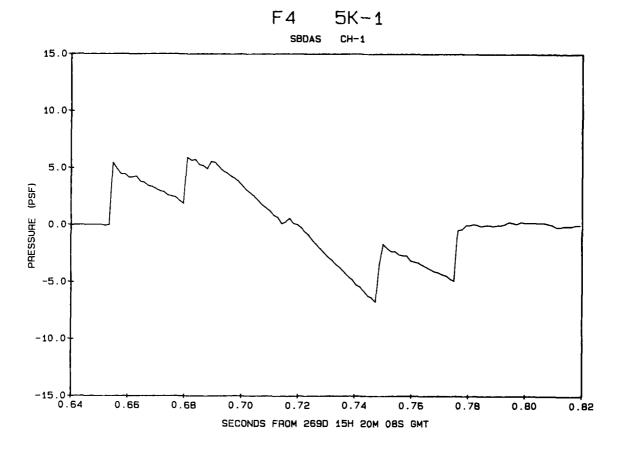
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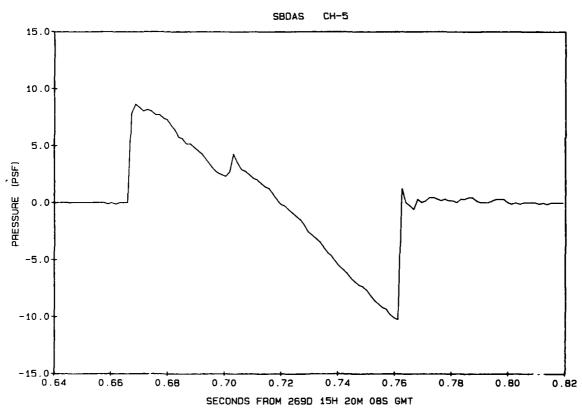
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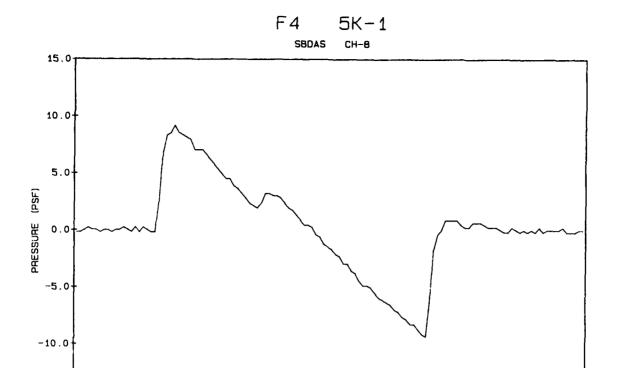
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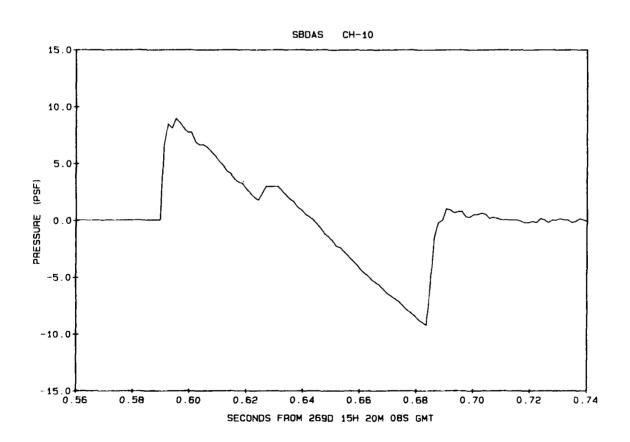
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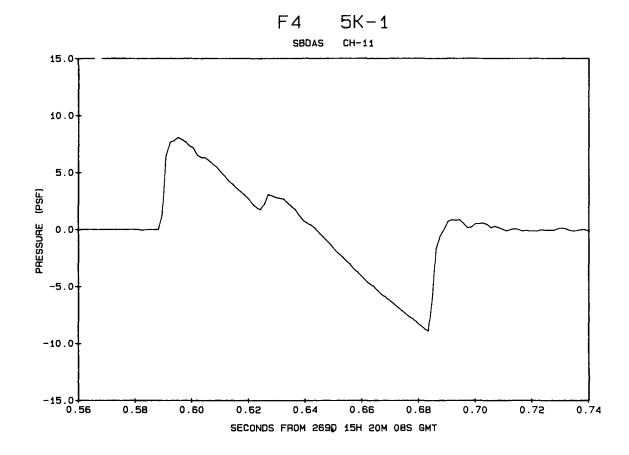
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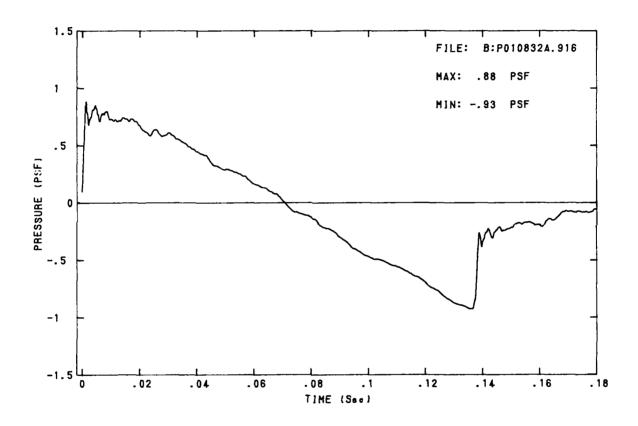
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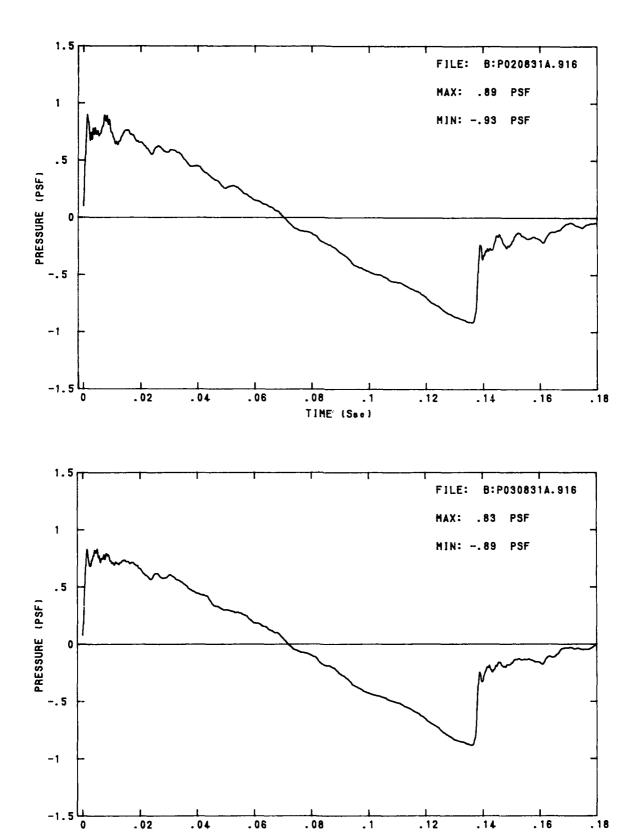
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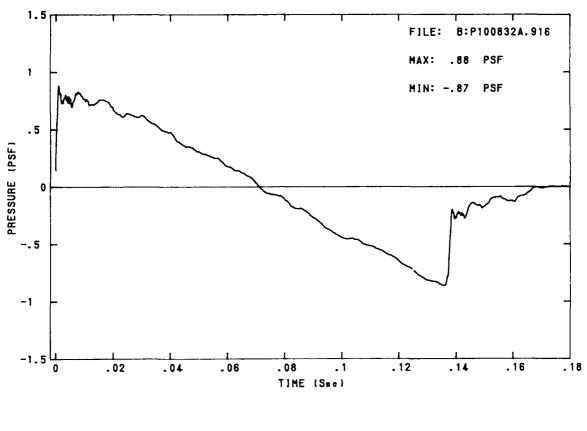


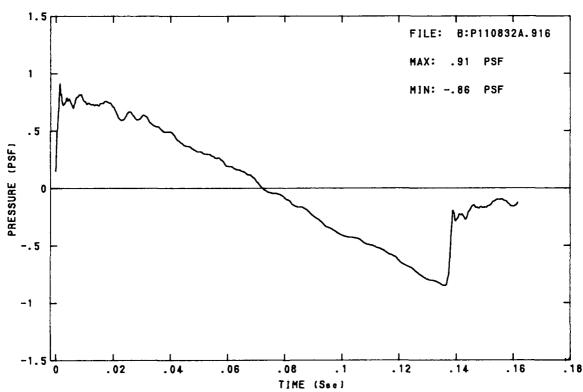
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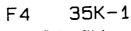


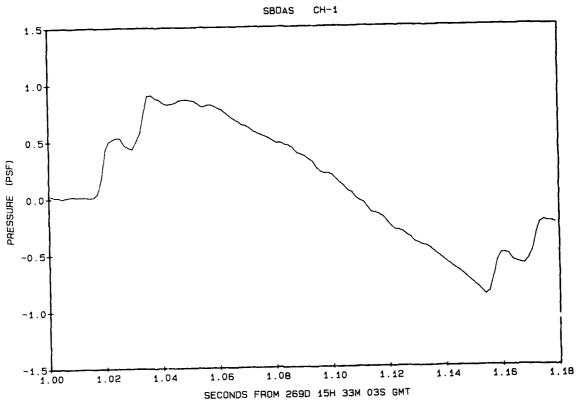


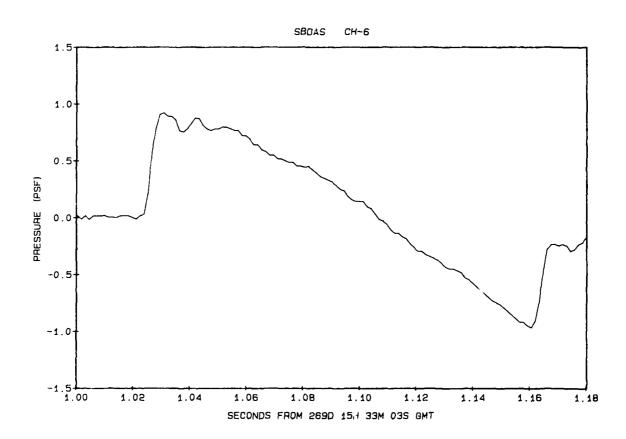
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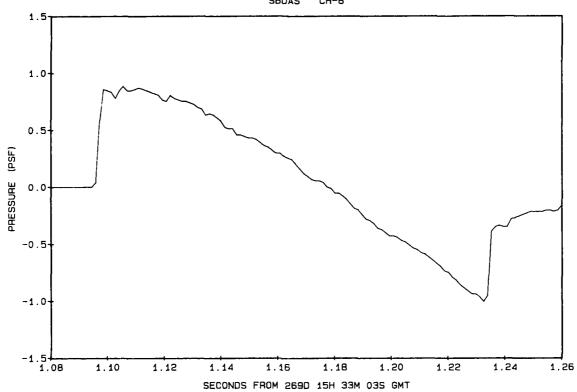




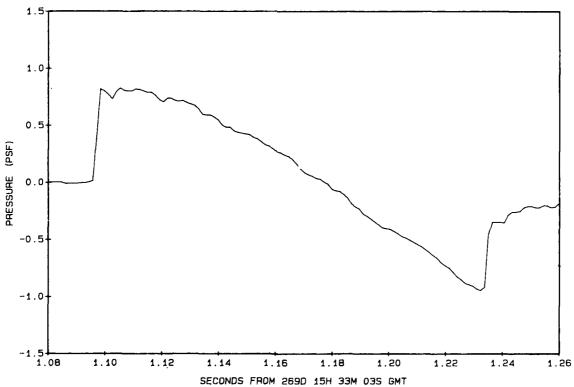


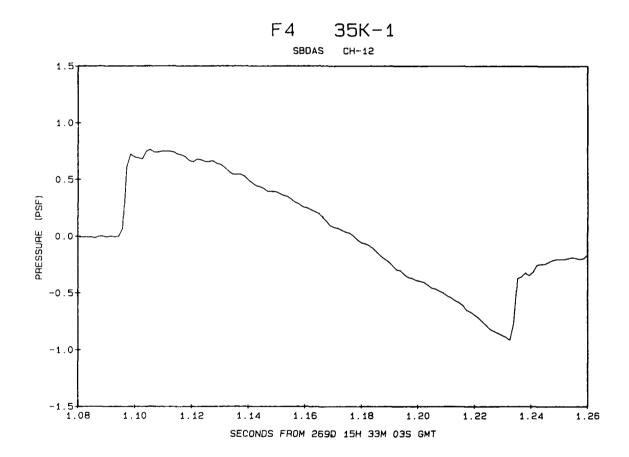
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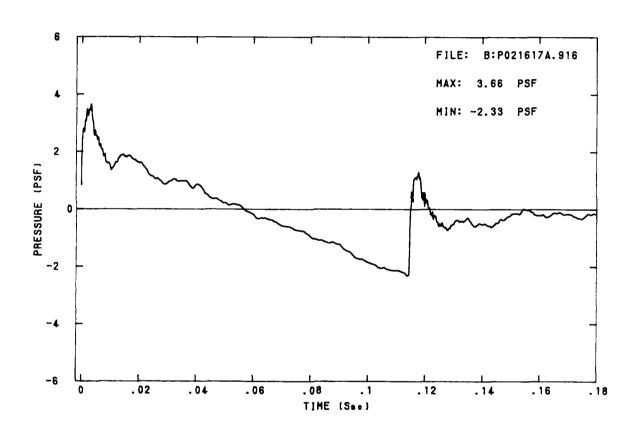


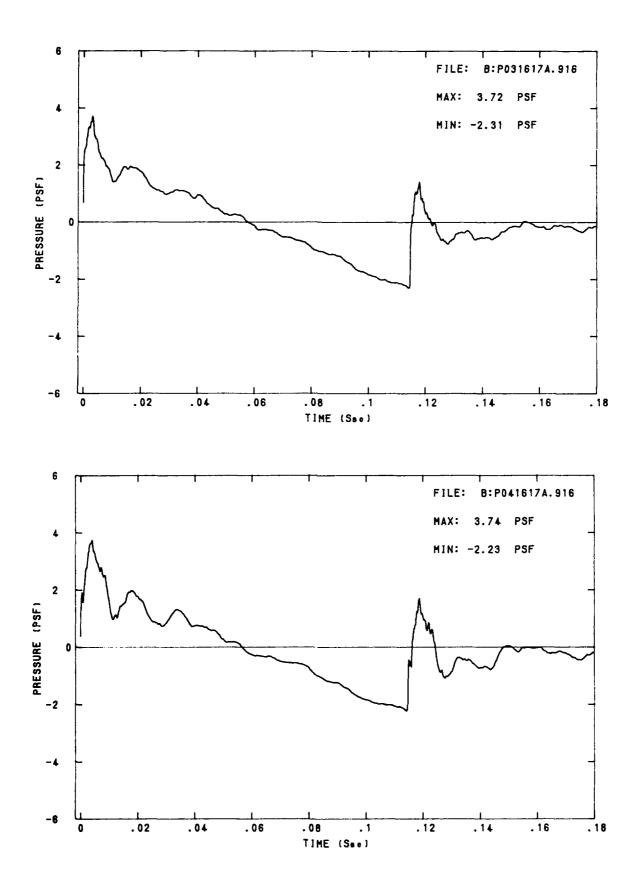


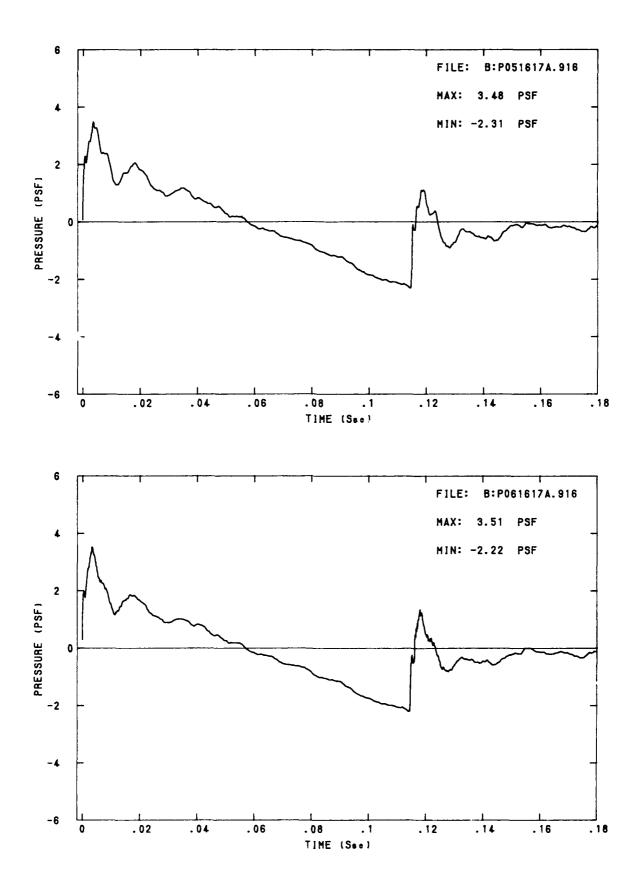


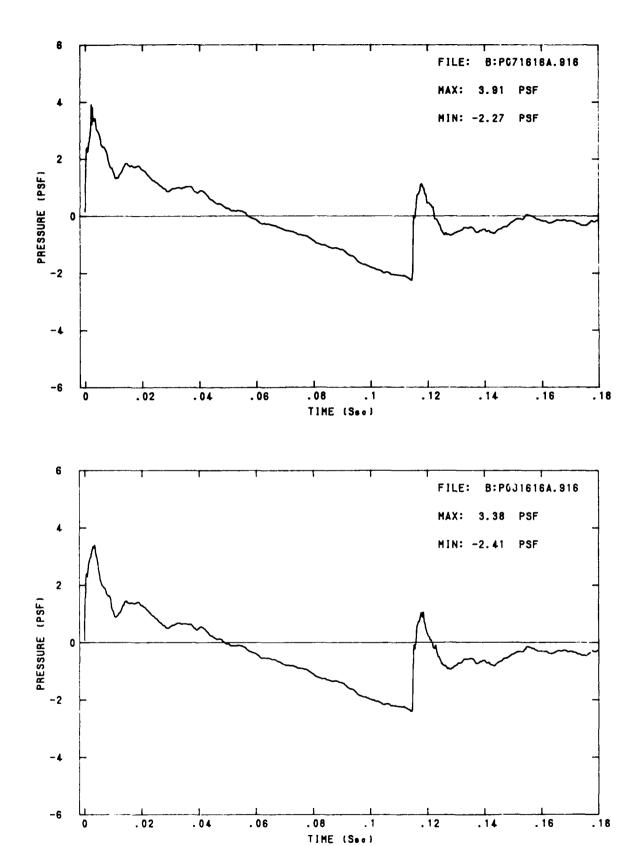


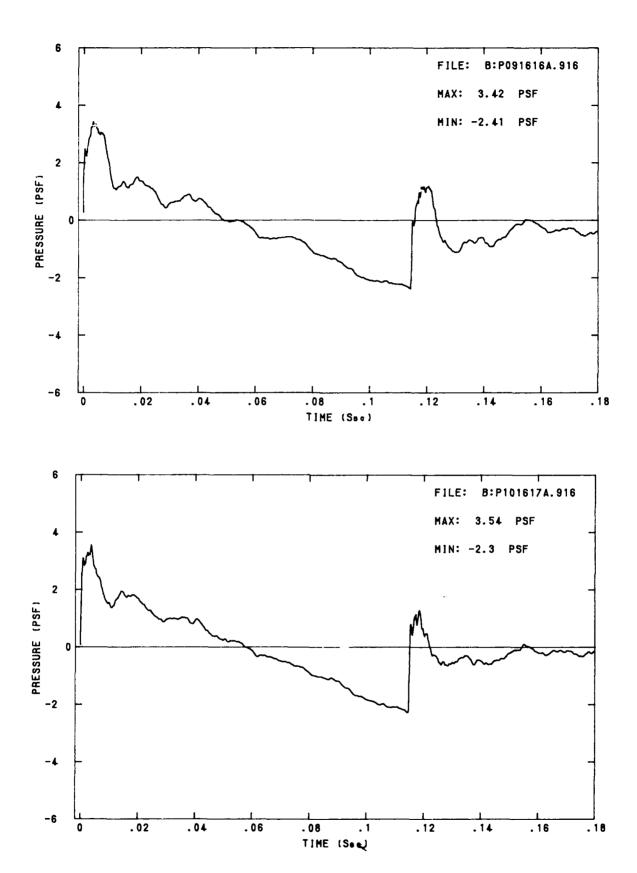
BOOM SIGNATURES from F-4 flying at 1.2 MACH, 20,700 ft AGL, and 0 ft. track offset occuring at 23:17:47 GMT, 16 Sep 86.

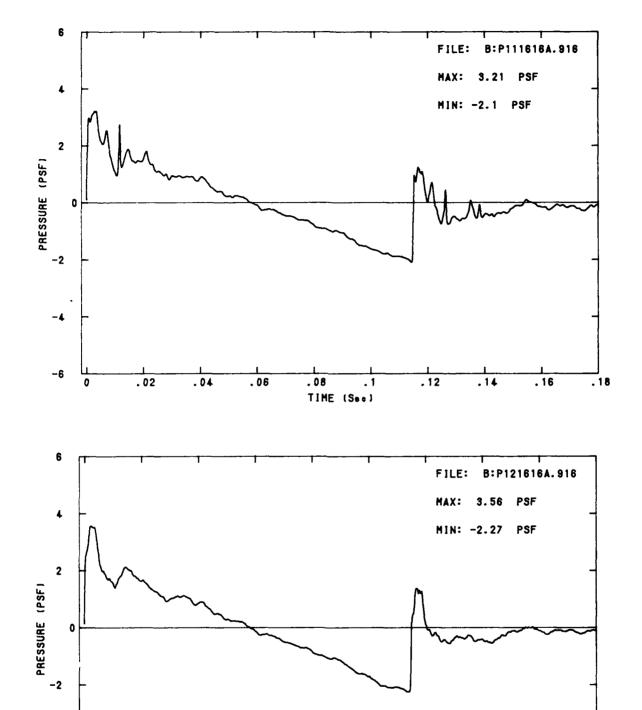












.08

TIME (See)

. 12

. 16

. 18

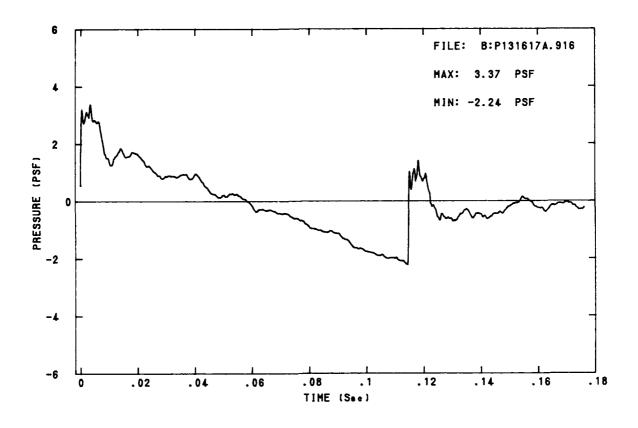
.04

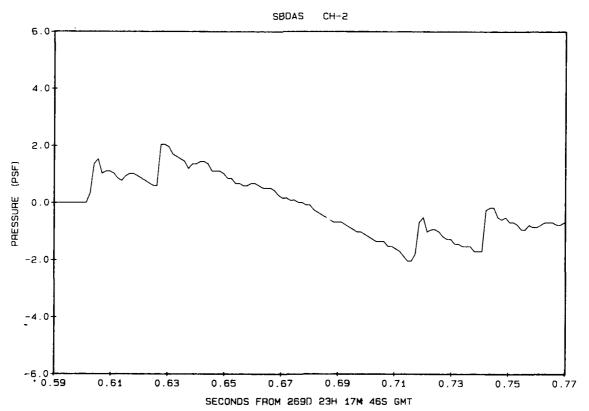
. 06

. 02

-4

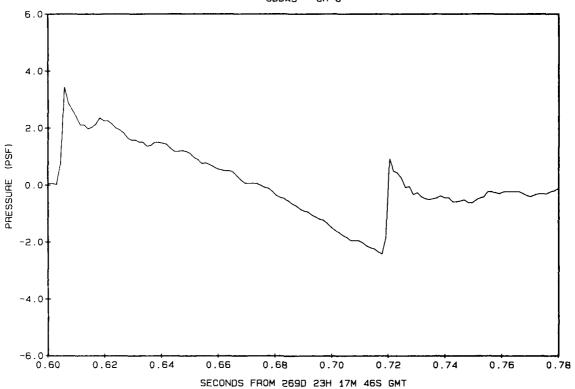
-6

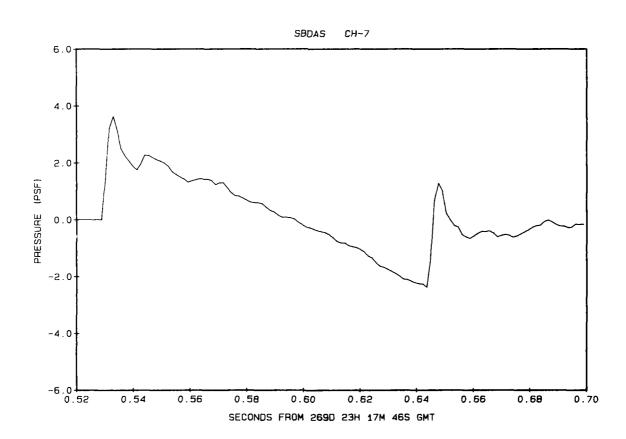


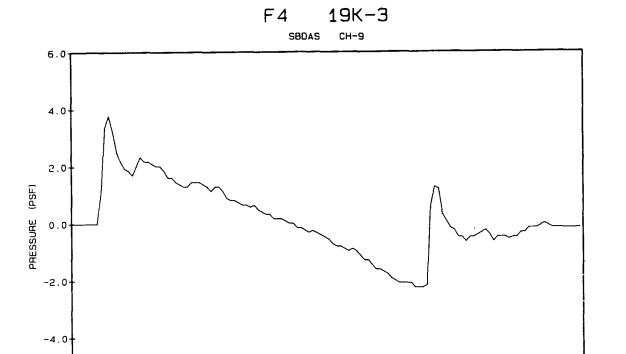


F4 19K-3









0.62

0.64

0.66

0.68

0.70

-6.0|-0.52

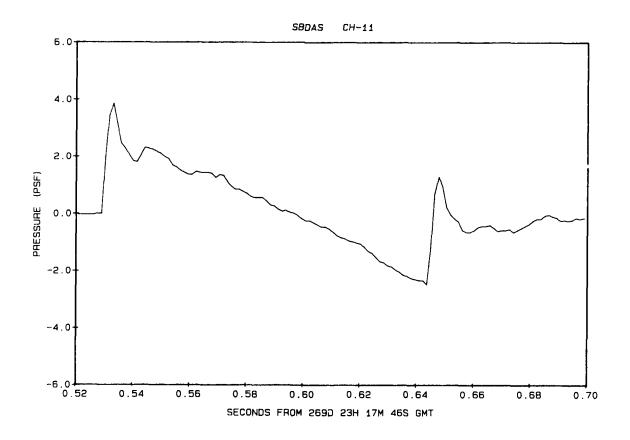
0.54

0.56

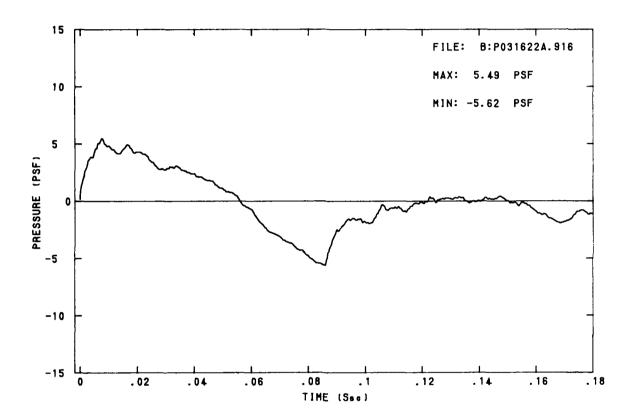
0.58

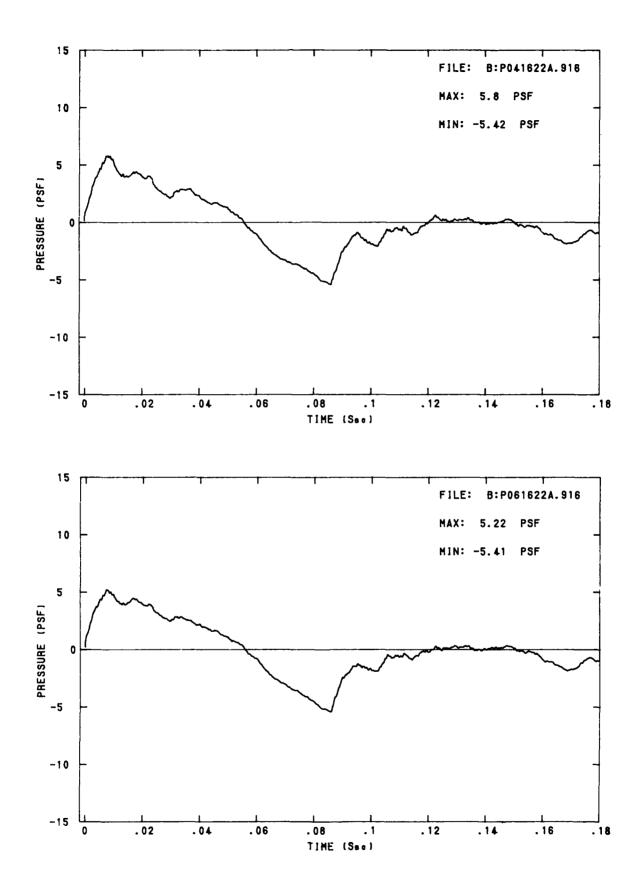
0.60

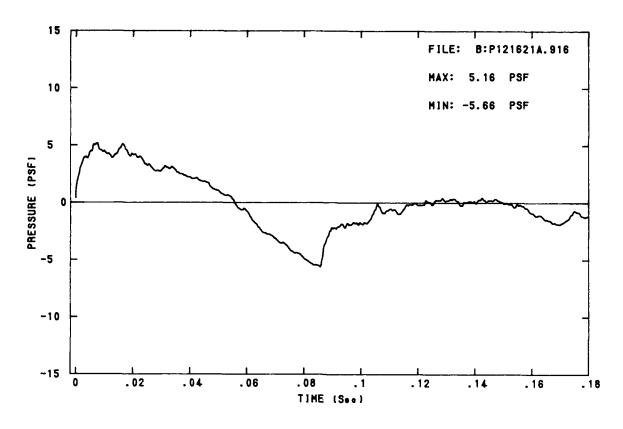
SECONDS FROM 269D 23H 17M 46S GMT

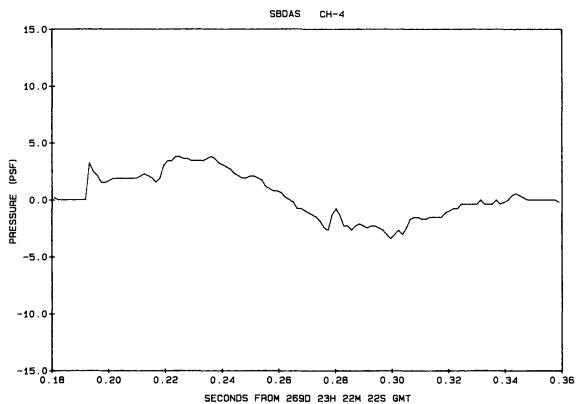


BOOM SIGNATURES from F-4 flying at 1.15 MACH, 5,500 ft AGL, and 0 ft. track offset occuring at 23:22:22 GMT, 16 Sep 86.

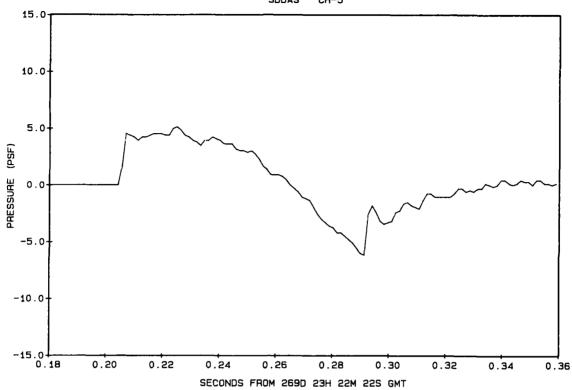


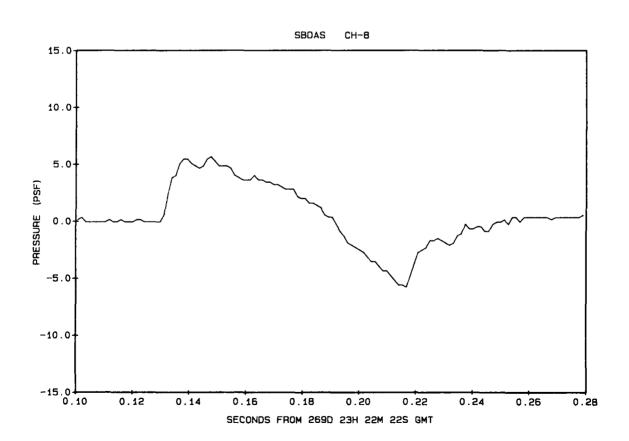




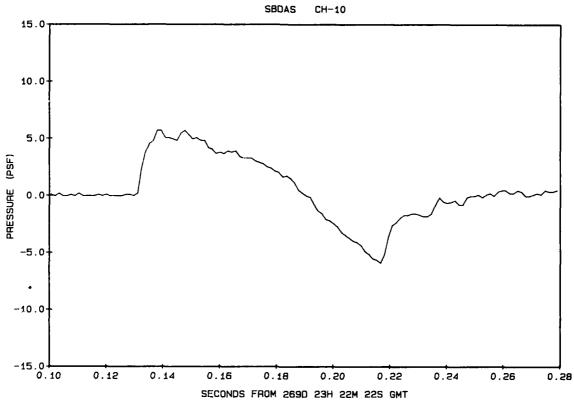


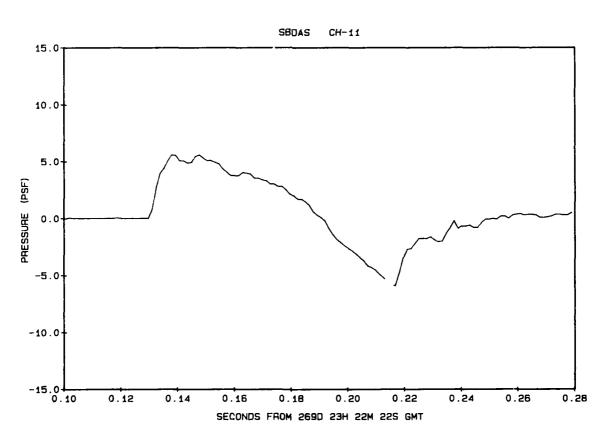




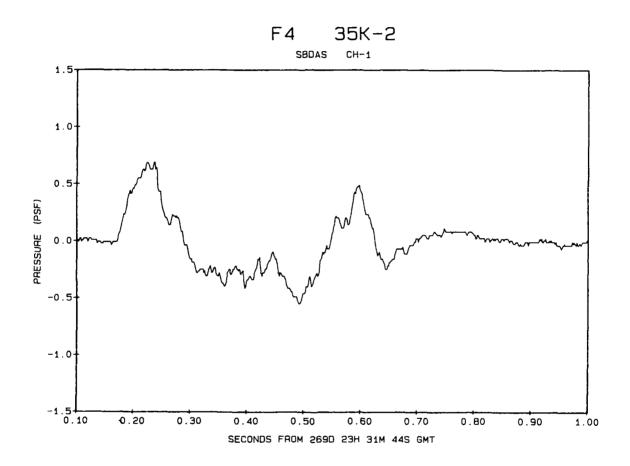


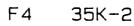


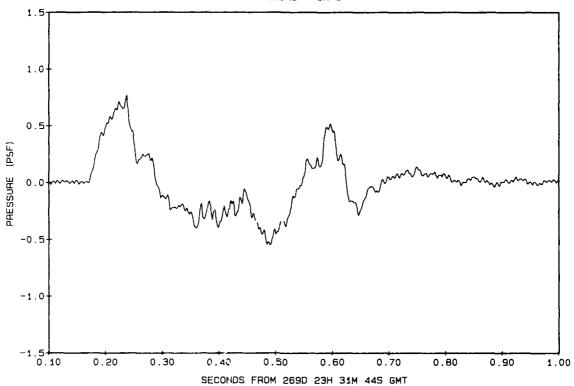


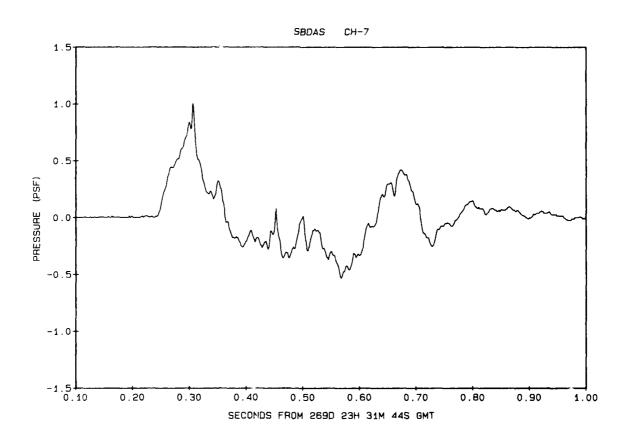


BOOM SIGNATURES from F-4 flying at 1.45 MACH, 35,100 ft AGL, and 60,600 ft. track offset occuring at 23:31:45 GMT, 16 Sep 86.

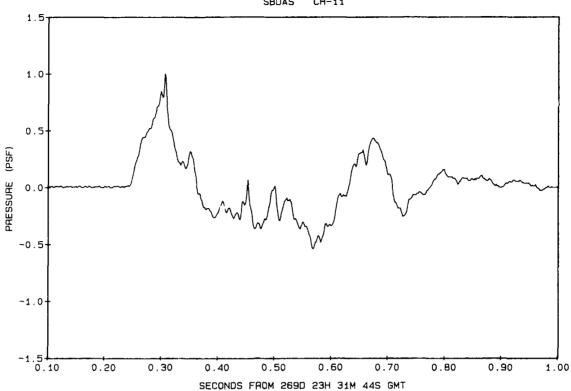


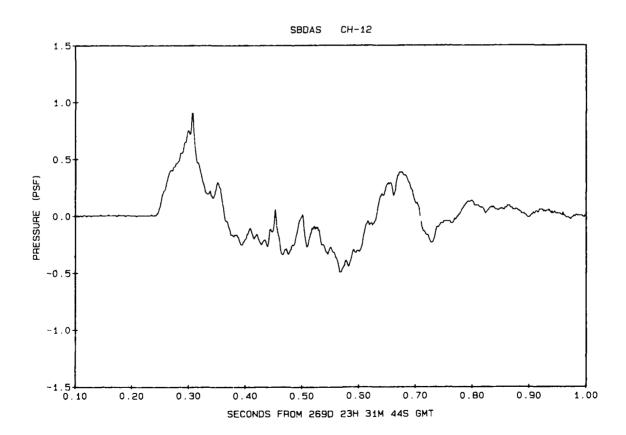




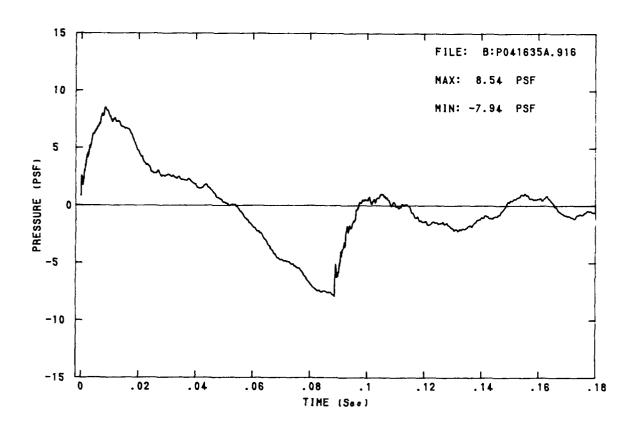


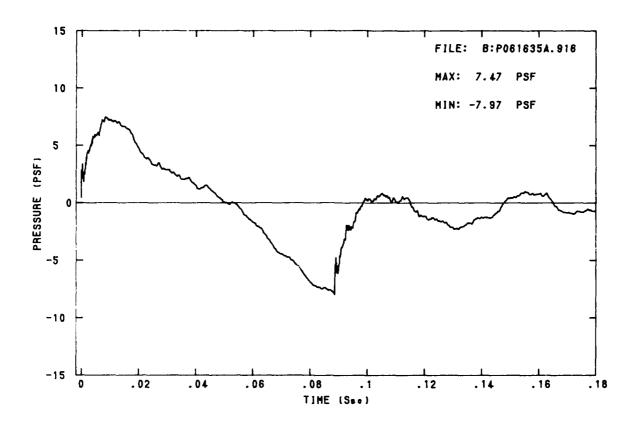
F4 35K-2

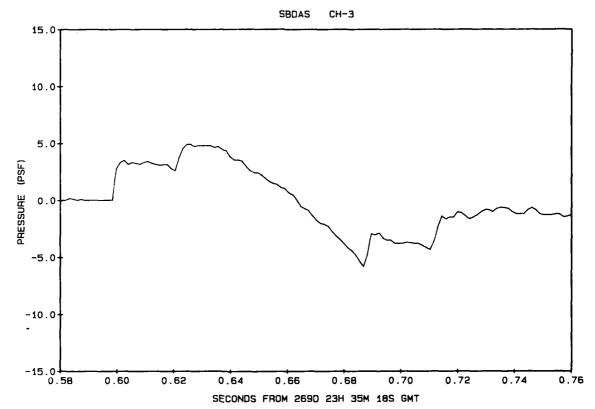




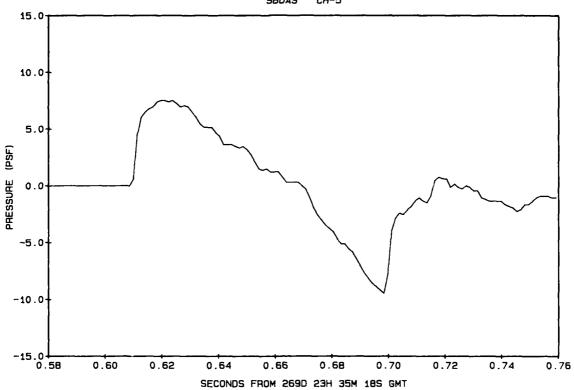
BOOM SIGNATURES from F-4 flying at 1.15 MACH, 5,200 ft AGL, and 0 ft. track offset occuring at 23:35:18 GMT, 16 Sep 86.

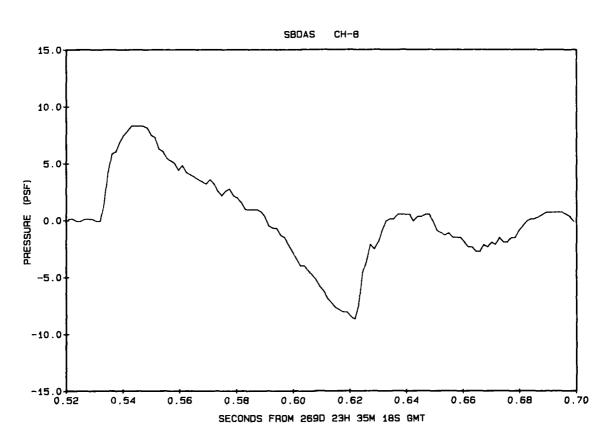




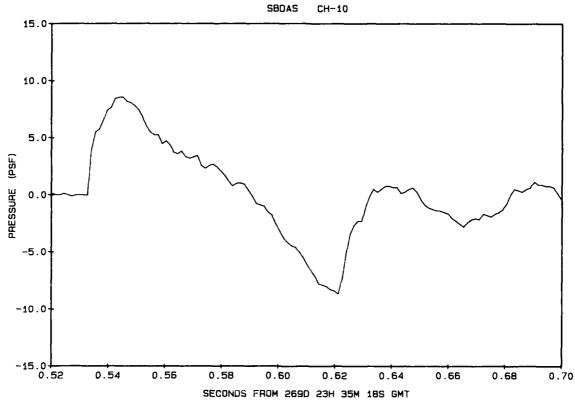


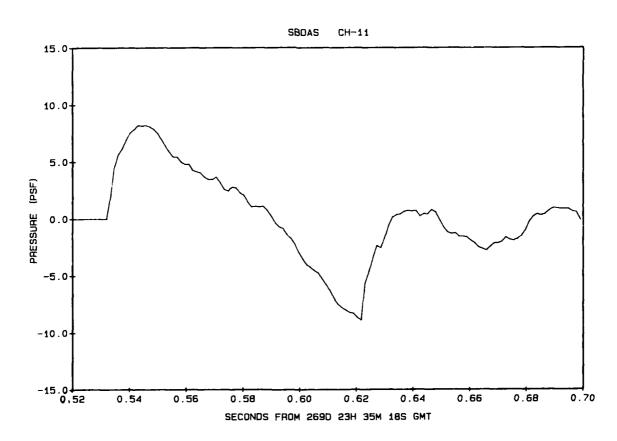
F4 5K-3



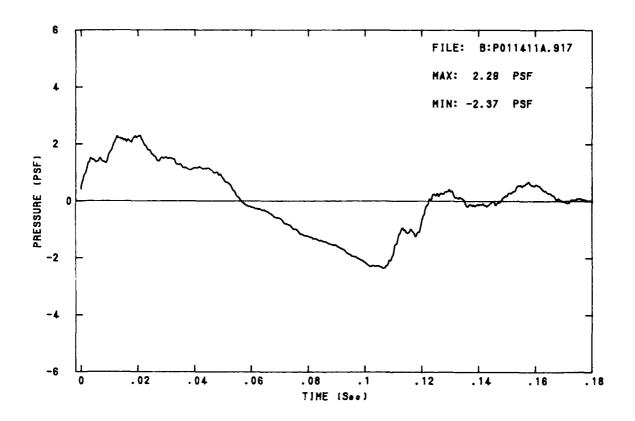


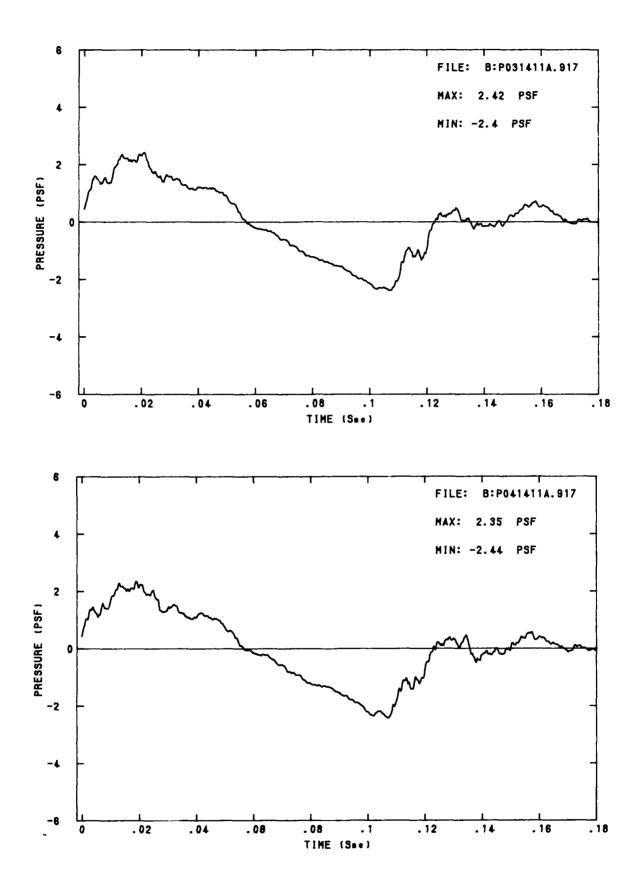
F4 5K-3

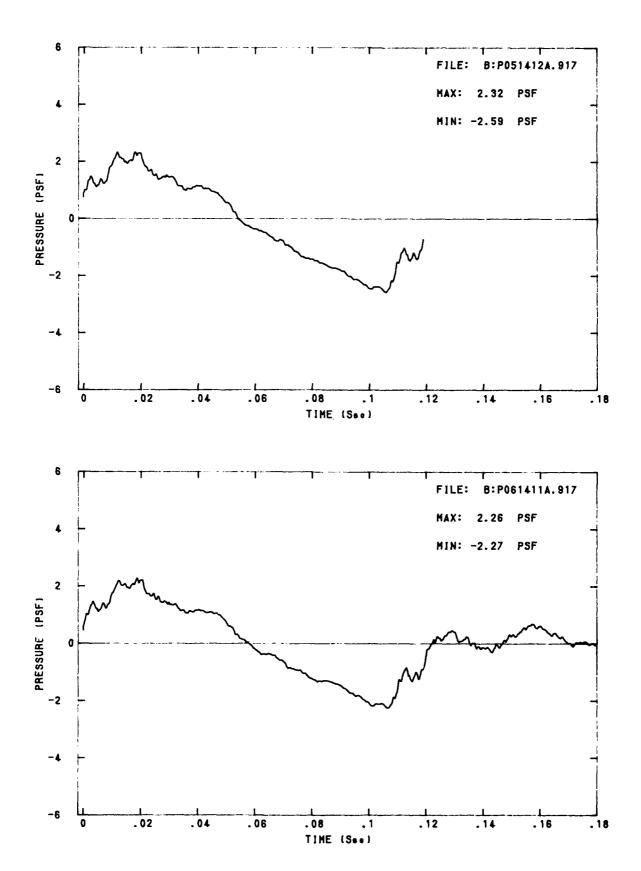


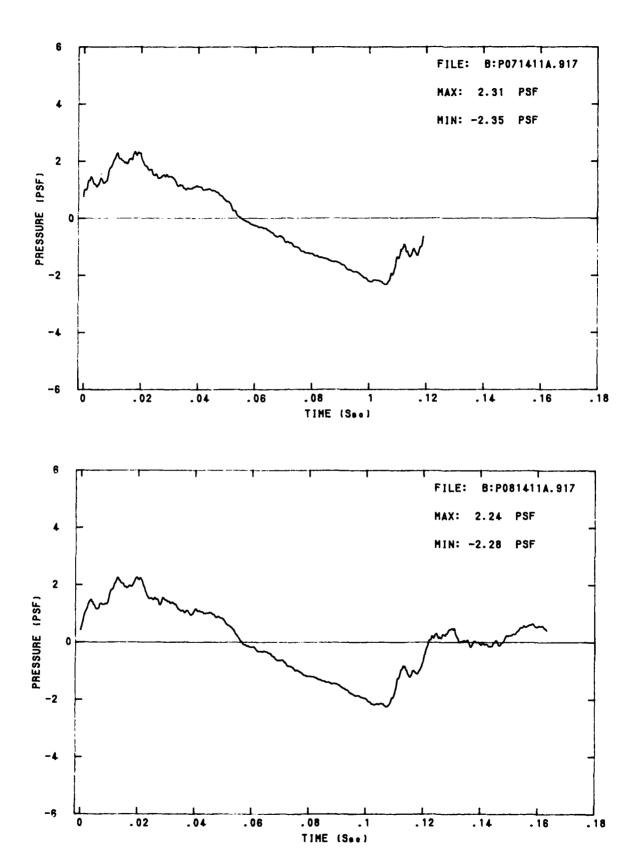


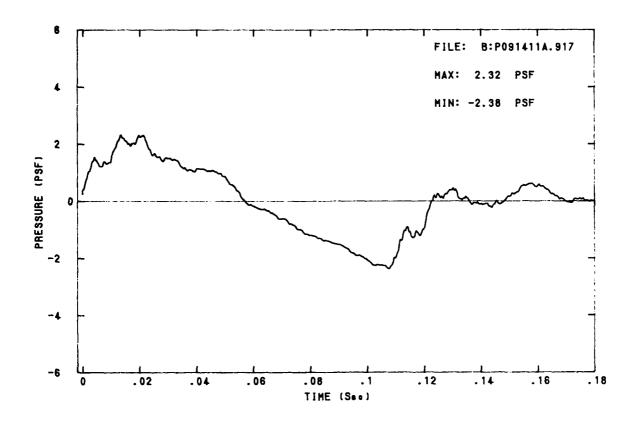
BOOM SIGNATURES from F-4 flying at 1.2 MACH, 19,000 ft AGL, and 0 ft. track offset occuring at 21:11:59 GMT, 17 Sep 86.

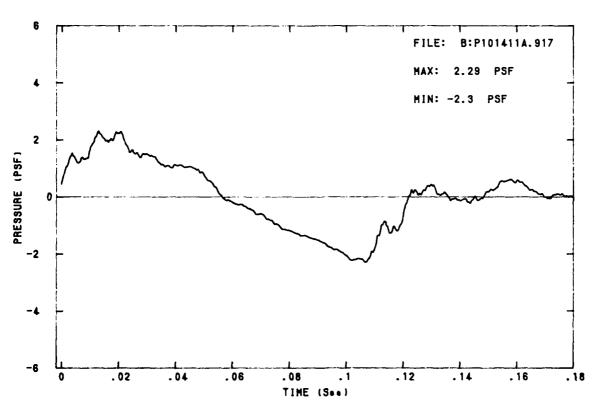




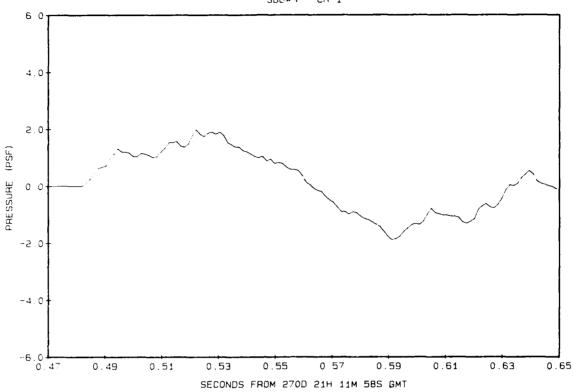


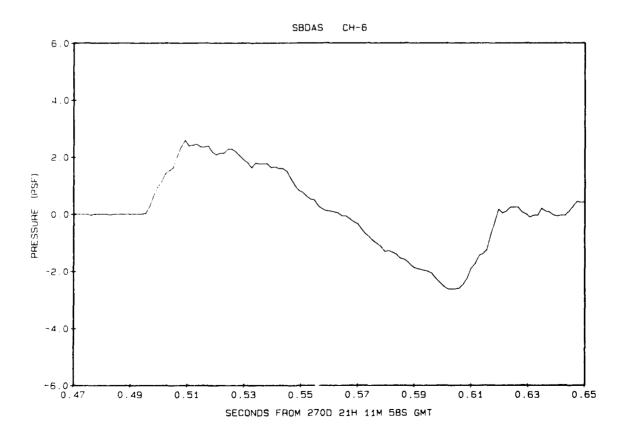




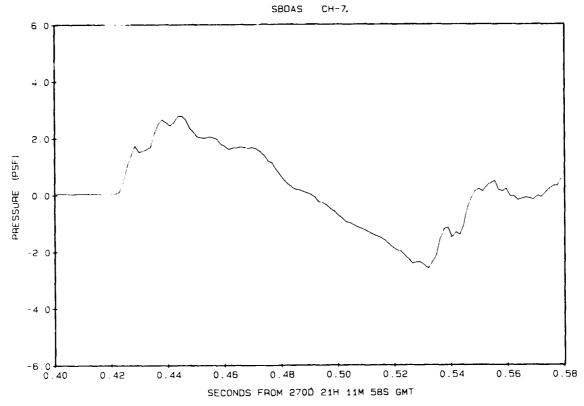


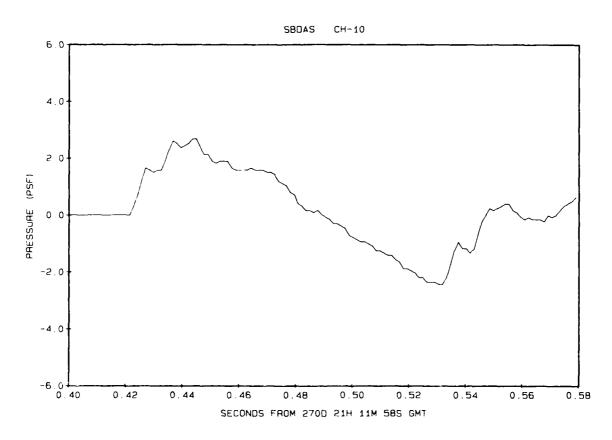
F4 19K-4



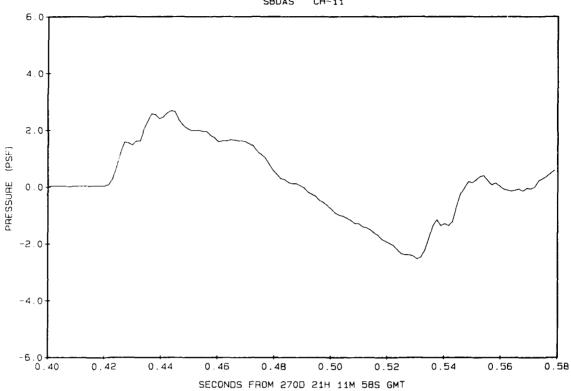


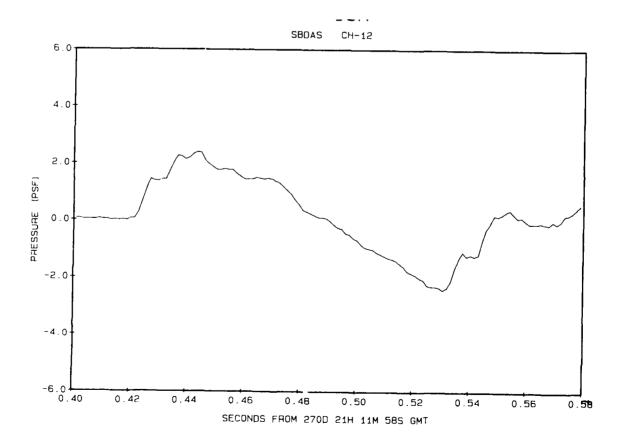
F4 19K-4
SBDAS CH-7.



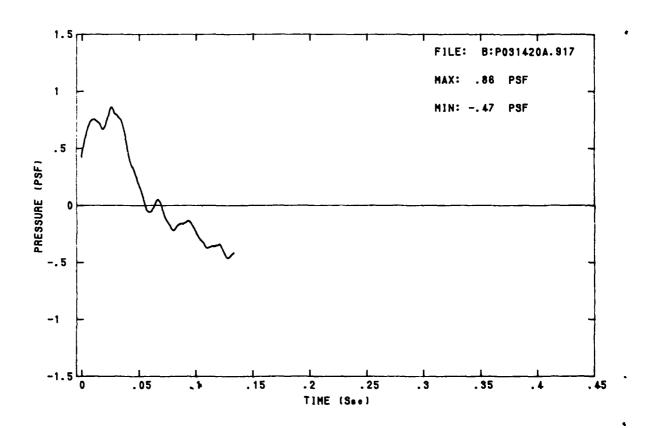


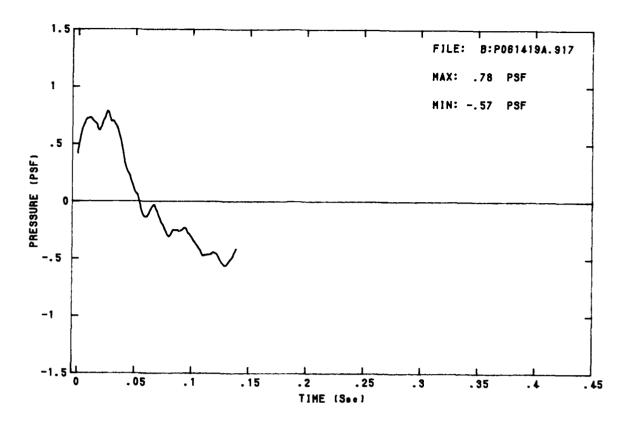
F4 19K-4

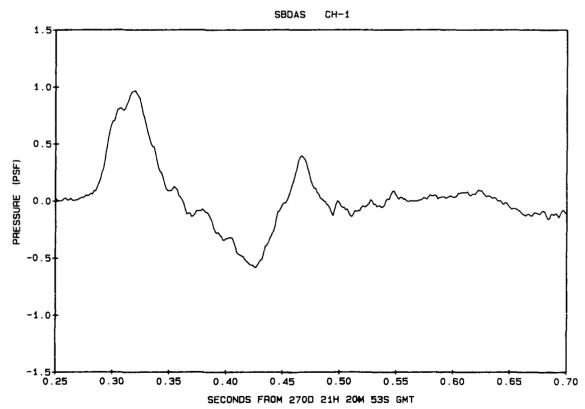




BOOM SIGNATURES from F-4 flying at 1.42 MACH, 34,900 ft AGL, and 60,000 ft. track offset occuring at 21:20:54 GMT, 17 Sep 86.

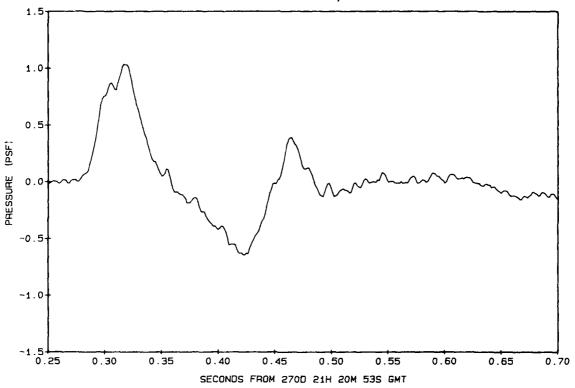


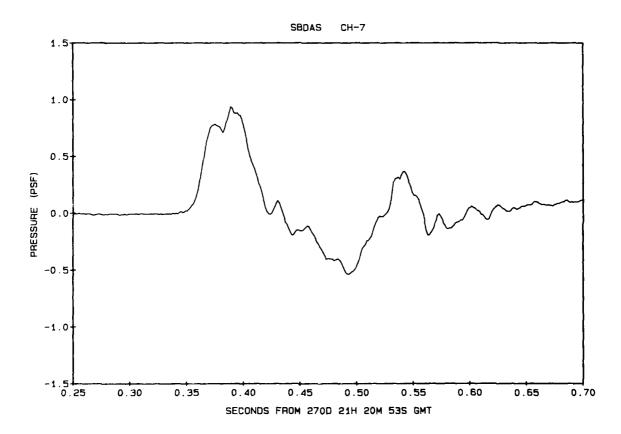




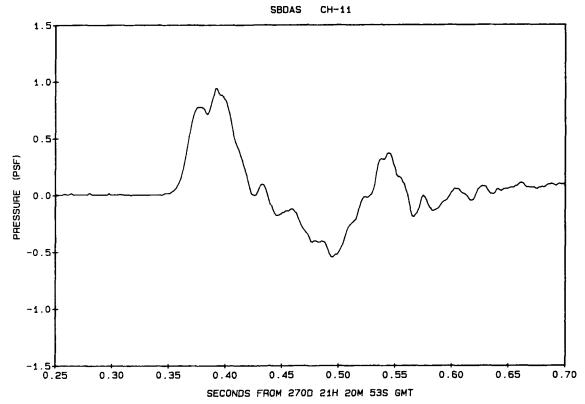
F4 35K-3

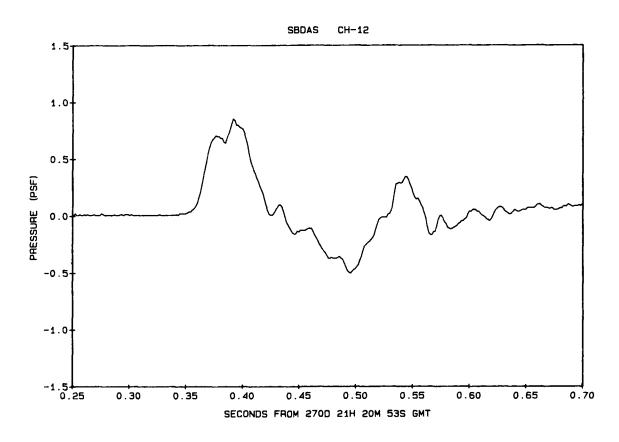
SBDAS CH-5



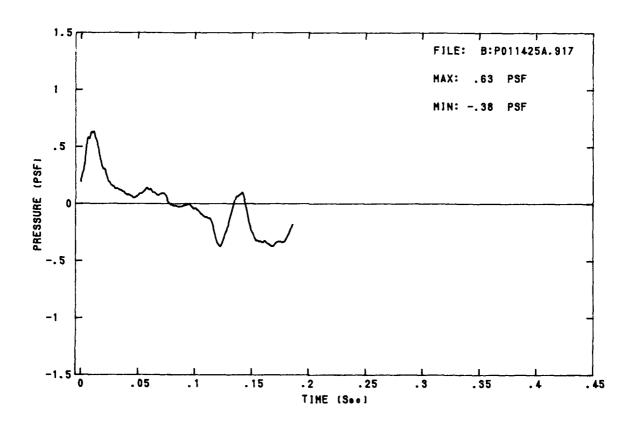


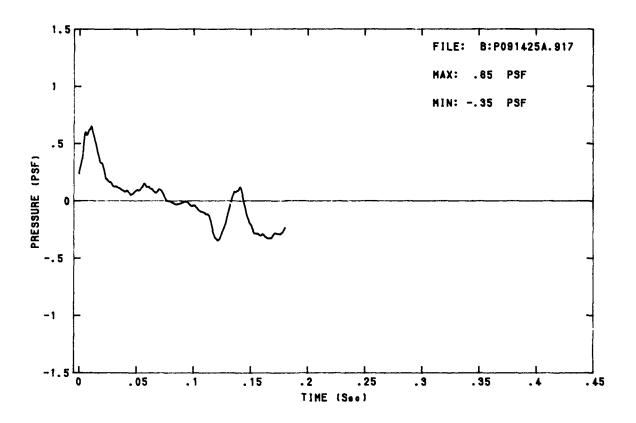
F4 35K-3

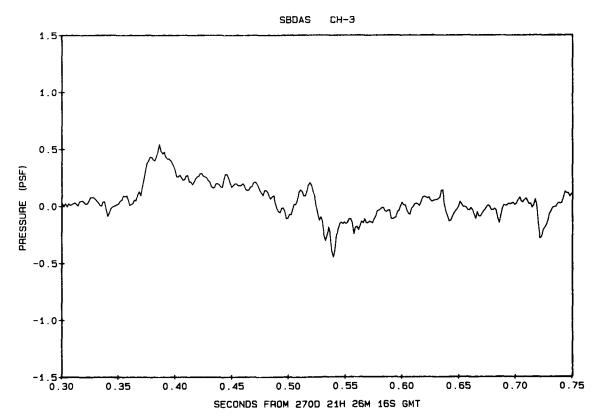


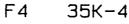


BOOM SIGNATURES from F-4 flying at 1.35 MACH, 35,200 ft AGL, and 60,000 ft. track offset occuring at 21:26:16 GMT, 17 Sep 86.

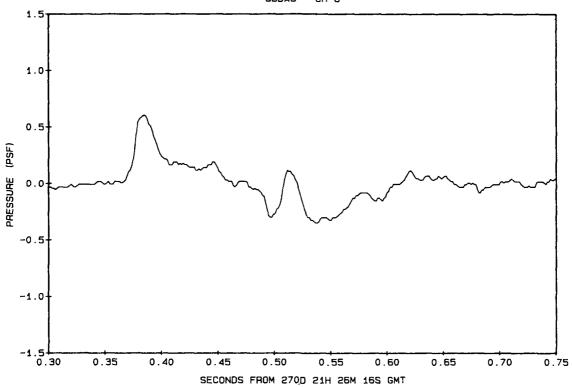


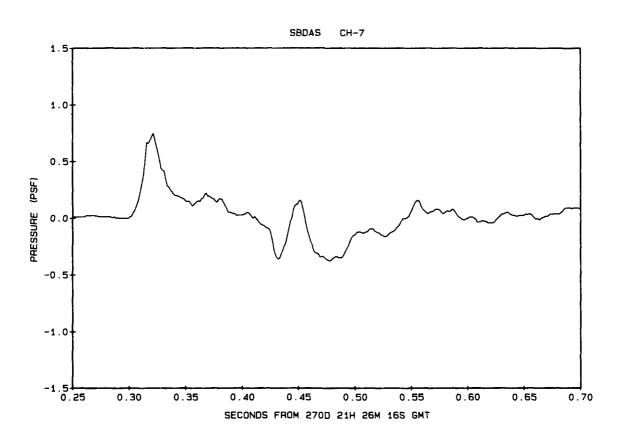


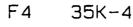




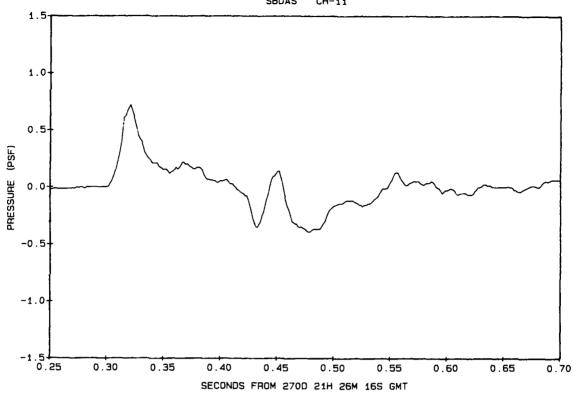
SBDAS CH-6

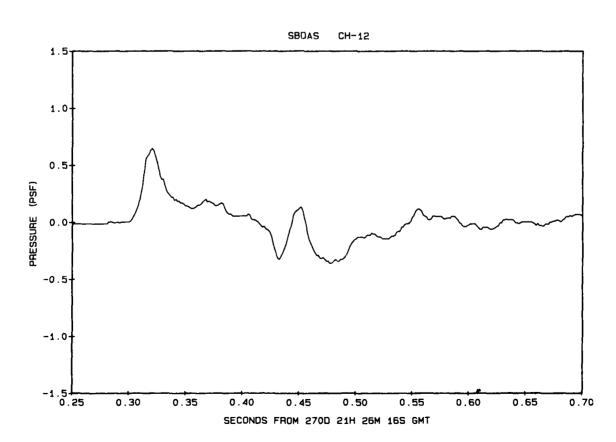




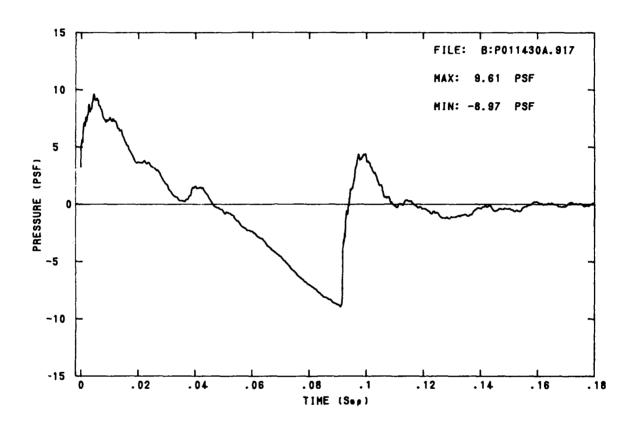


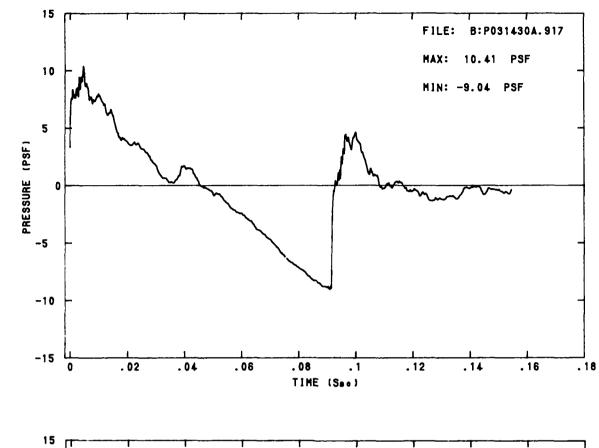


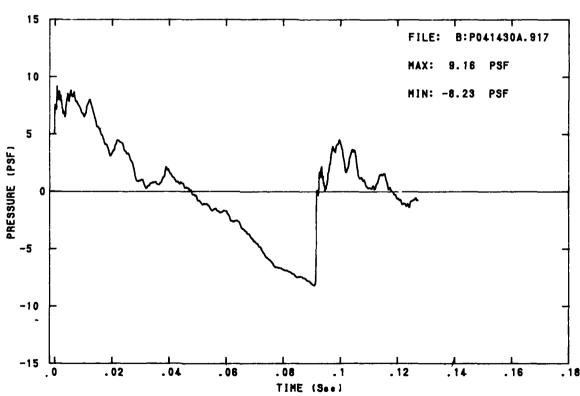


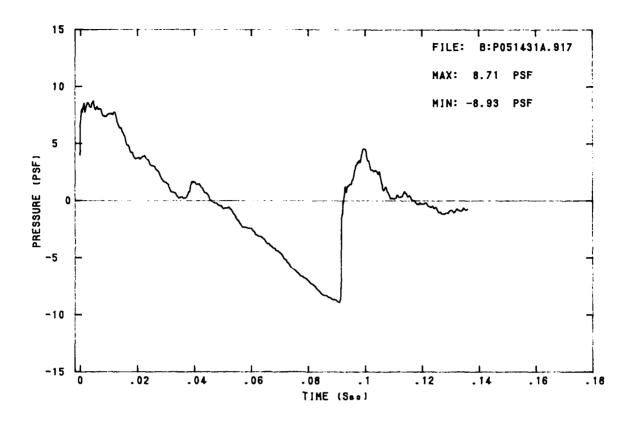


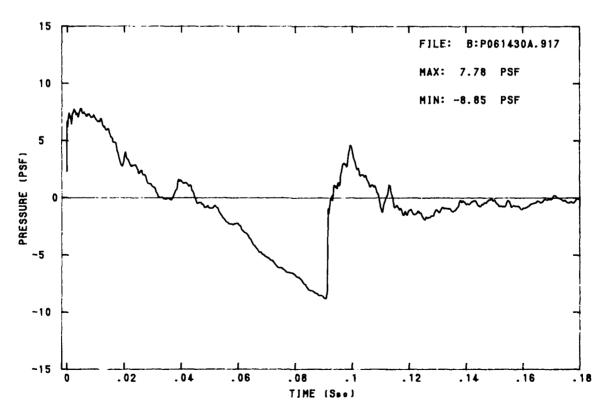
BOOM SIGNATURES from F-4 flying at 1.13 MACH, 5,700 ft AGL, and 0 ft. track offset occuring at 21:31:08 GMT, 17 Sep 86.

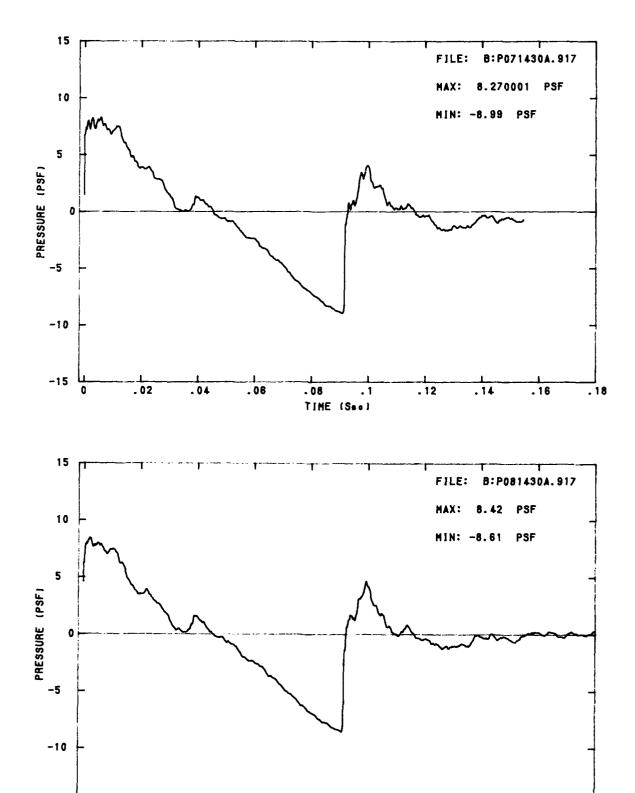












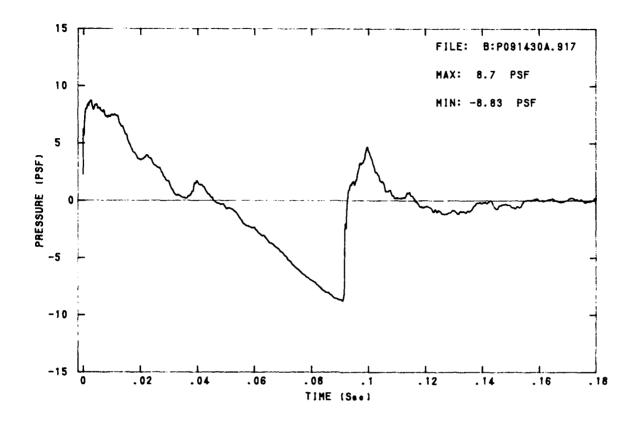
. 08

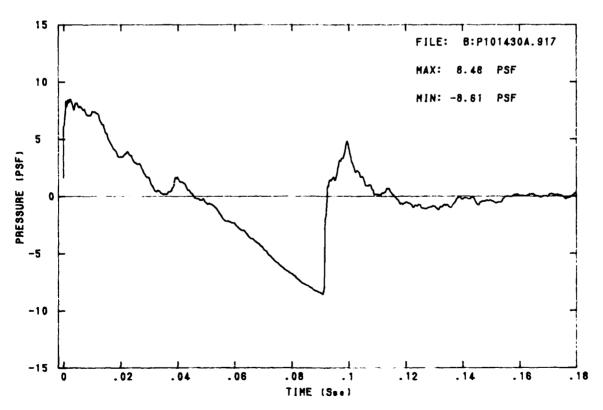
TIME (See)

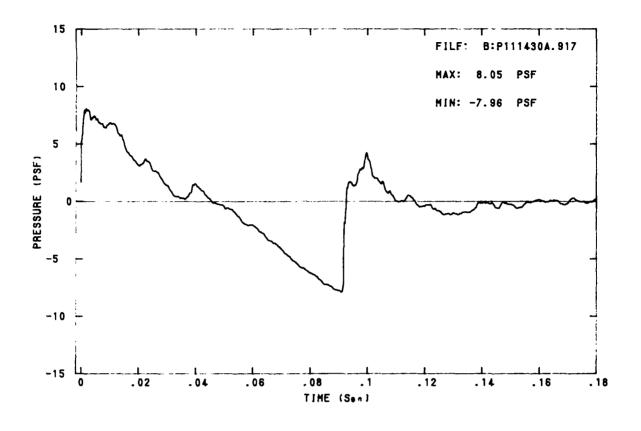
. 18

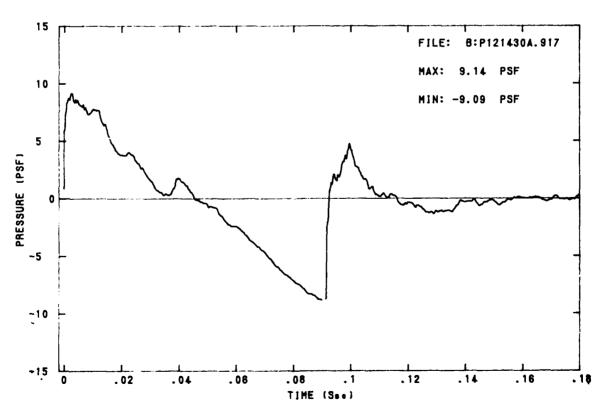
.06

-15

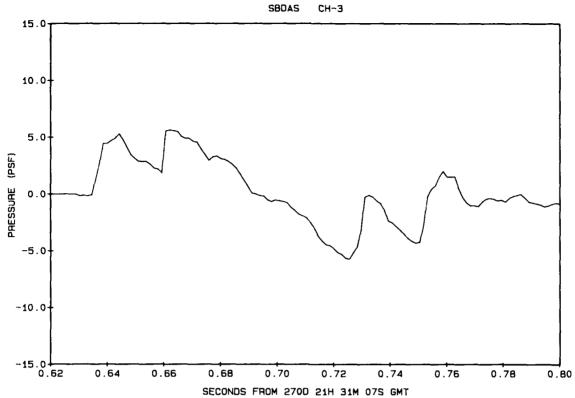


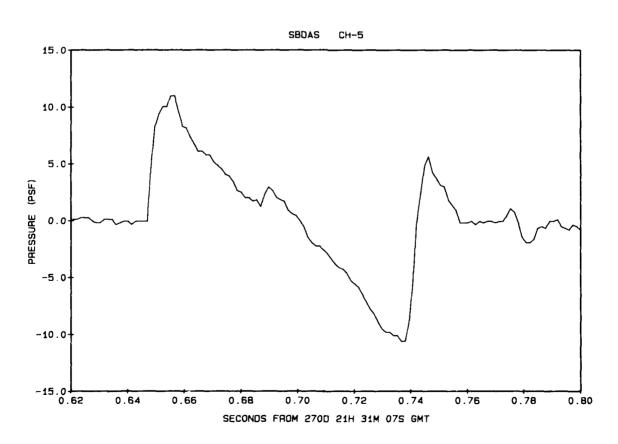


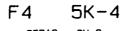


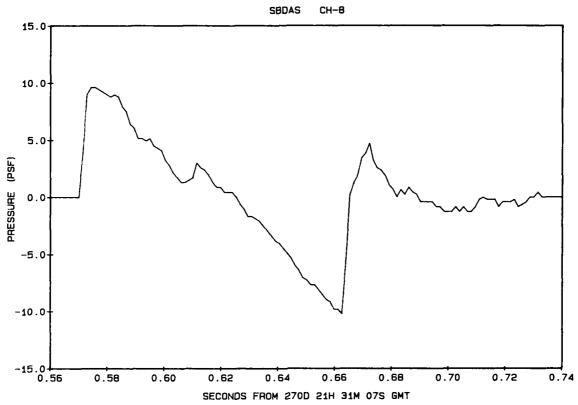


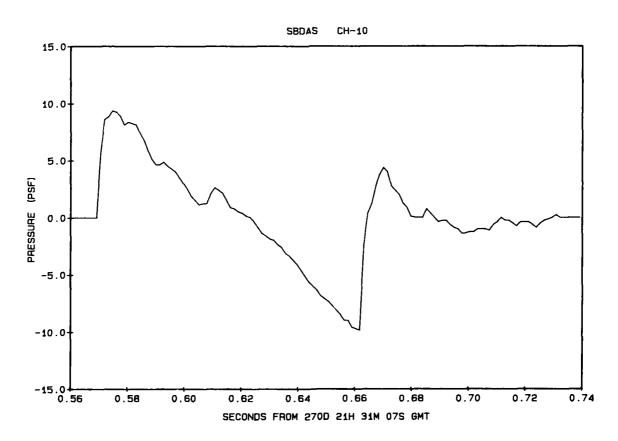
F4 5K-4

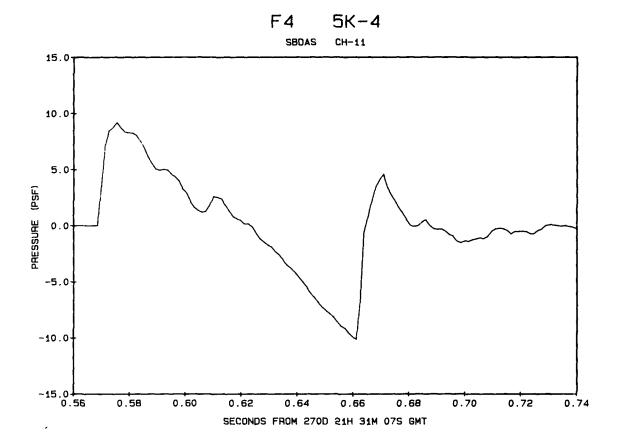




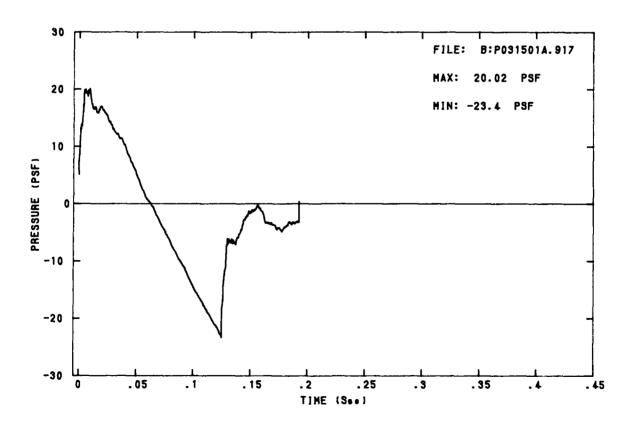


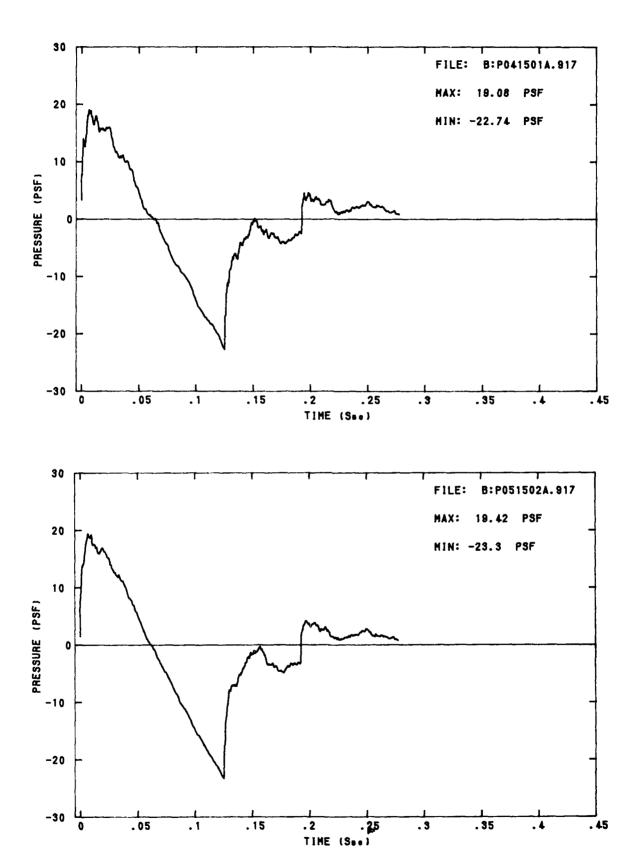


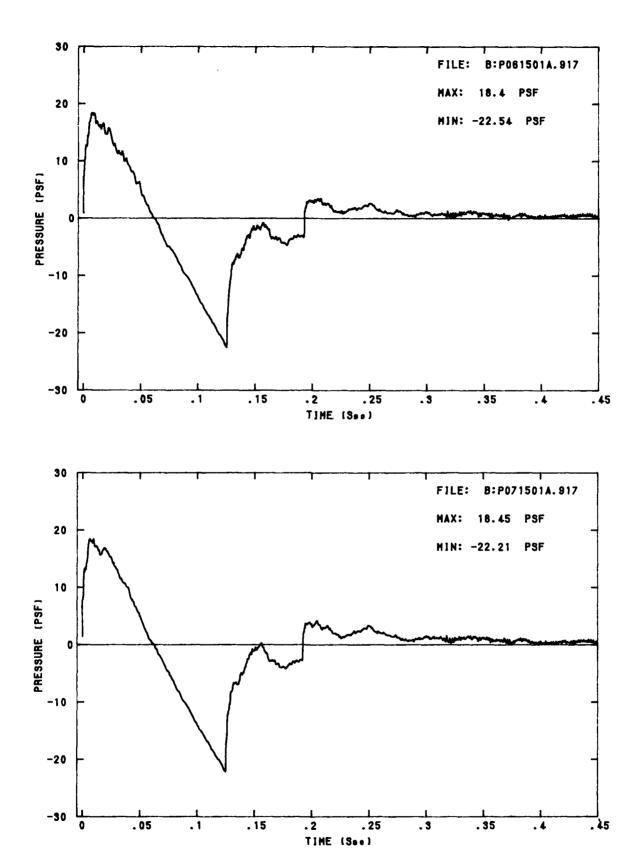


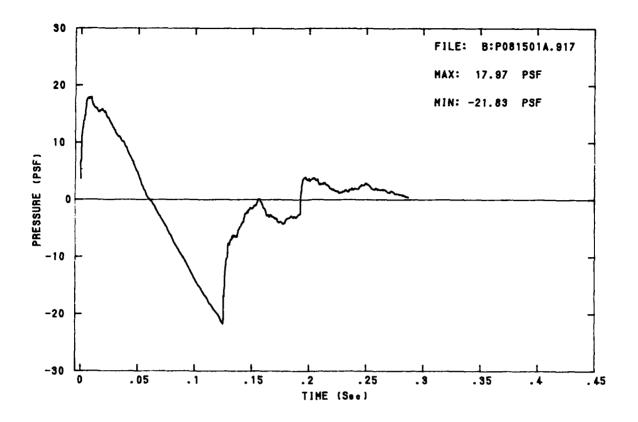


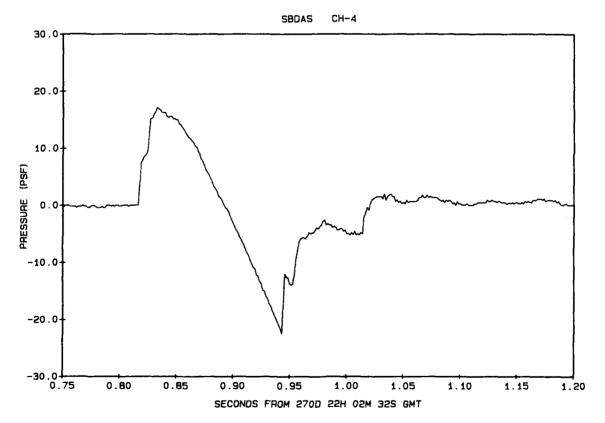
BOOM SIGNATURES from F-111A Flying at 1.03 MACH, 1,200 ft AGL, and 0 ft. track offset occuring at 22:02:33 GMT, 17 Sep 86.



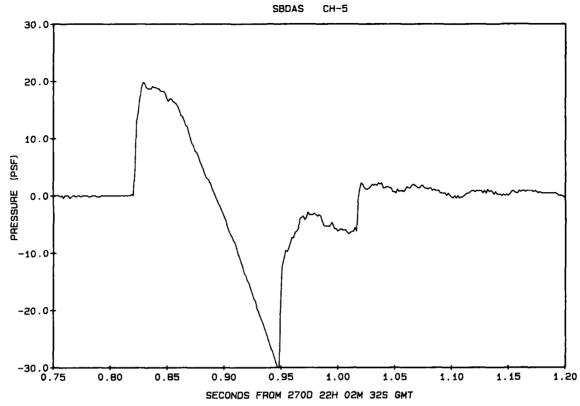


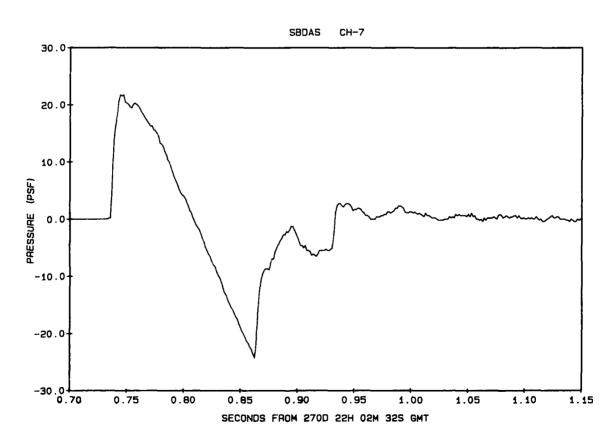




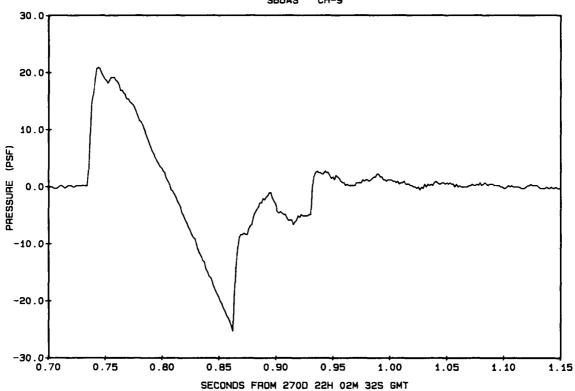


F111 1K-1

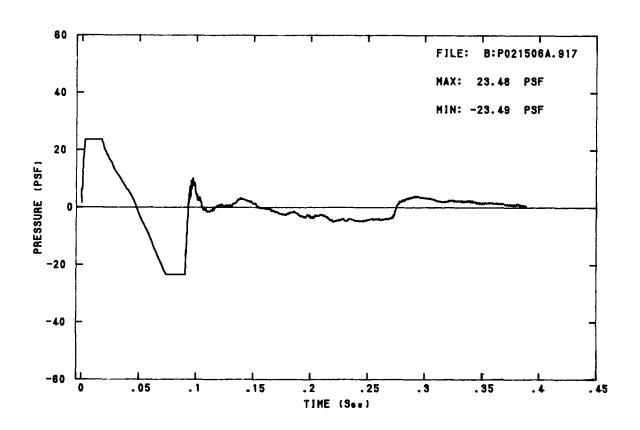


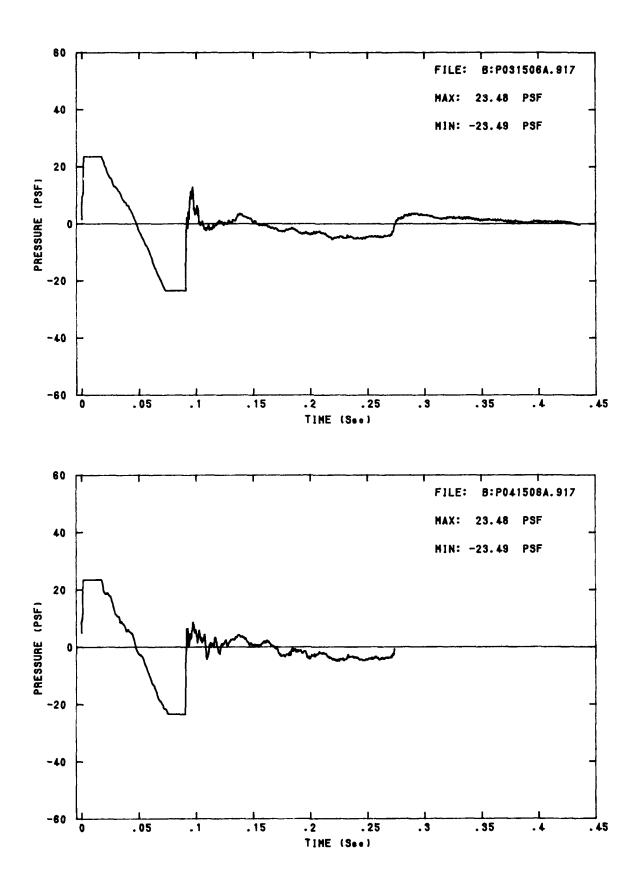


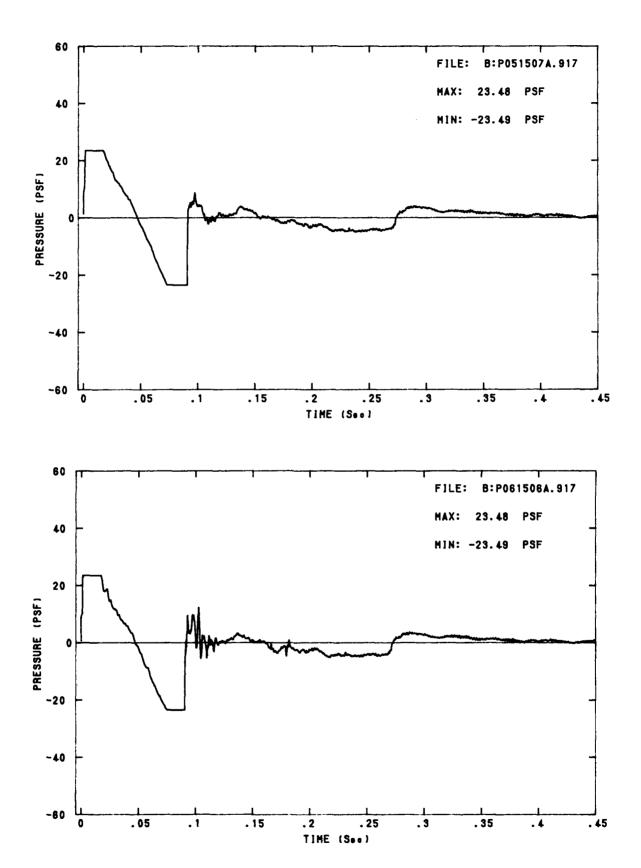
F111 1K-1
SBDAS CH-9

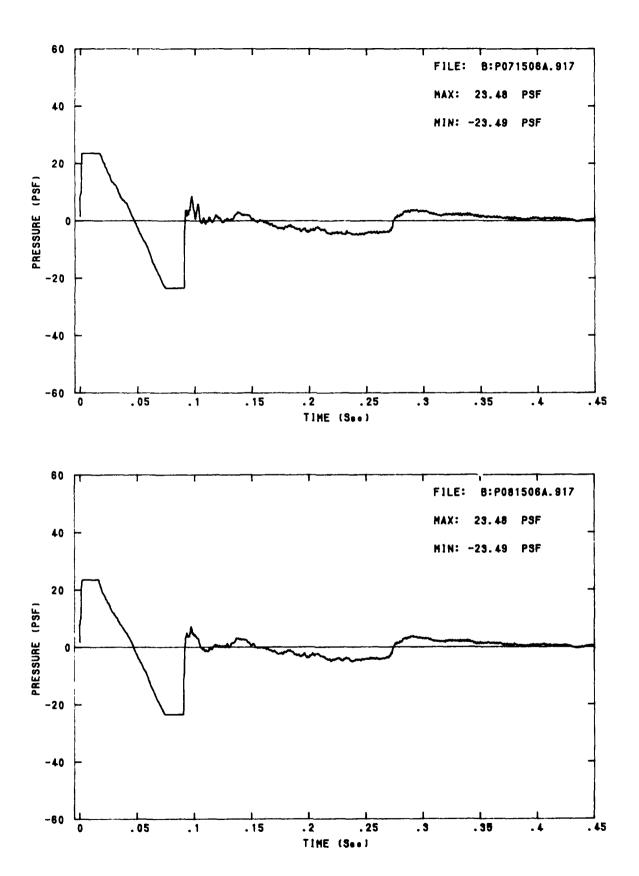


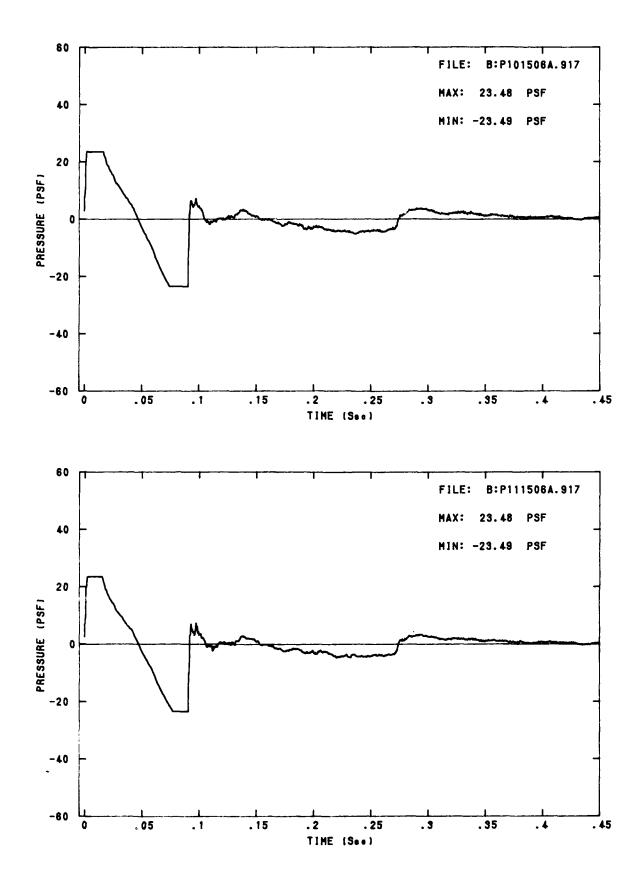
BOOM SIGNATURES from F-111A Flying at 1.04 MACH, 1,200 ft AGL, and 0 ft. track offset occuring at 22:07:49 GMT, 17 Sep 86.

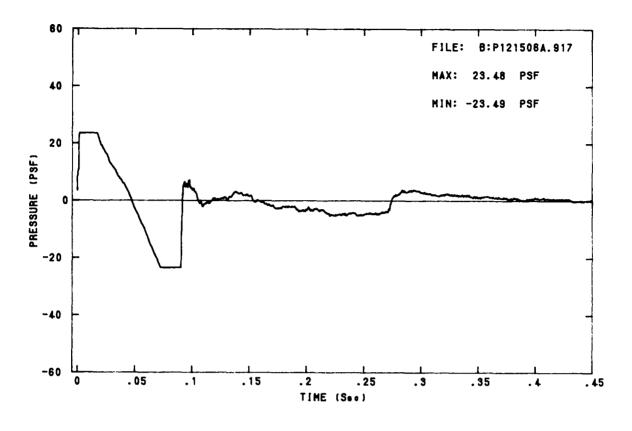


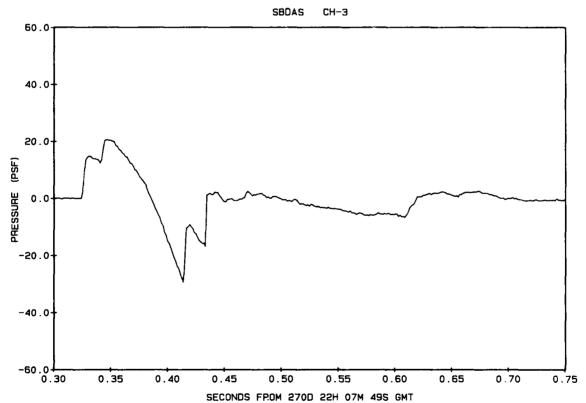




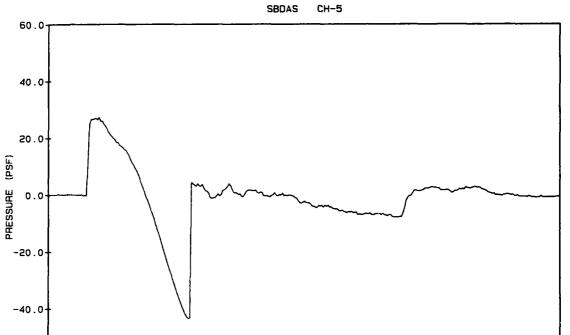








F111 1K-2



0.50

0.55

SECONDS FROM 270D 22H 07M 49S GMT

0.60

0.65

0.70

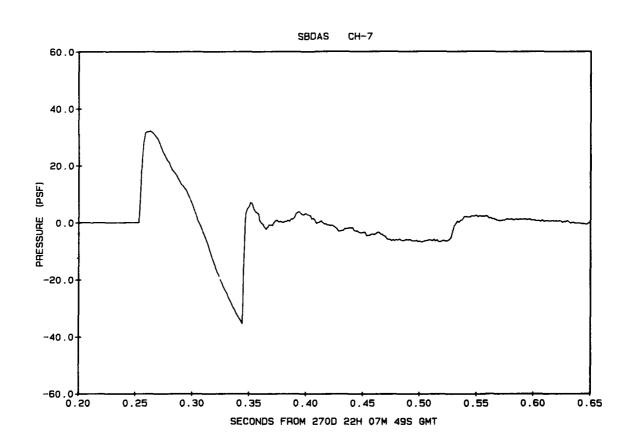
0.75

-60.01

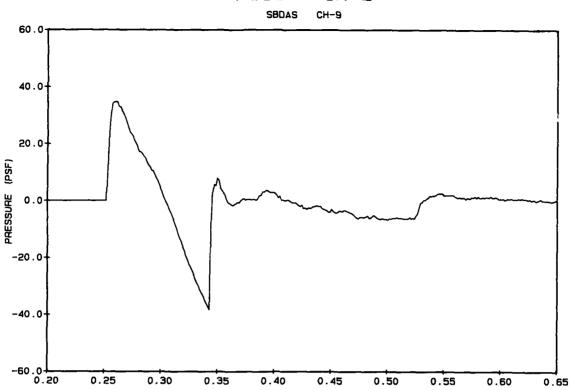
0.35

0.40

0.45

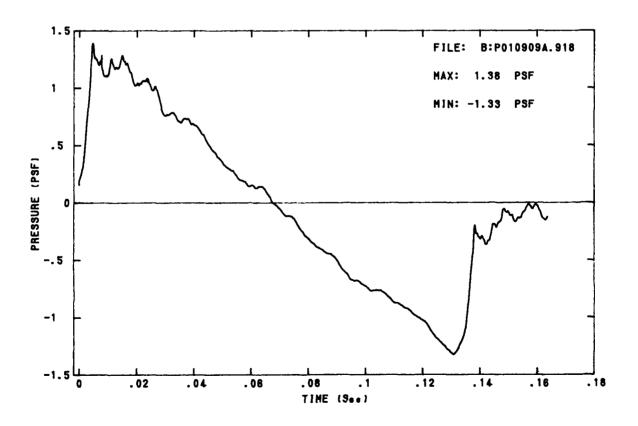


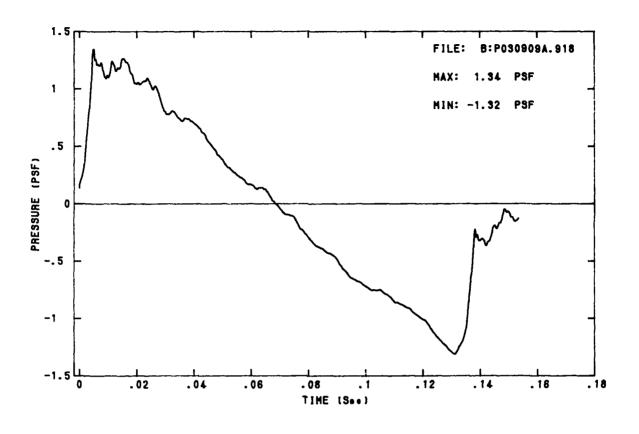
F111 1K-2

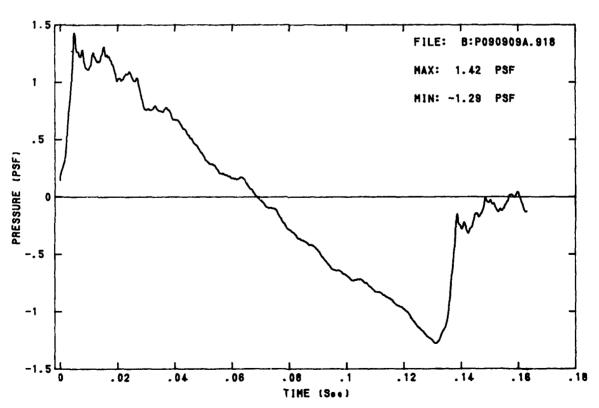


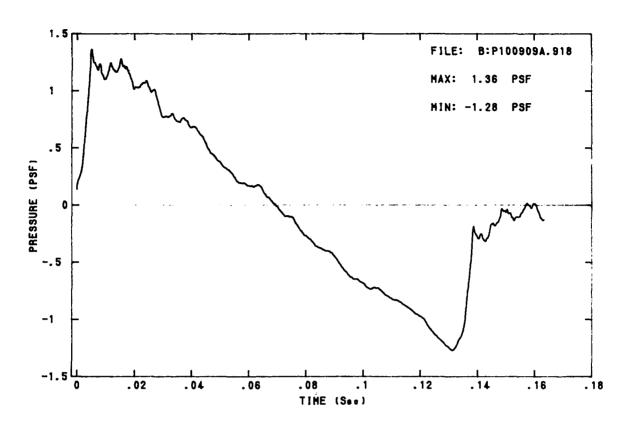
SECONDS FROM 270D 22H 07M 49S GMT

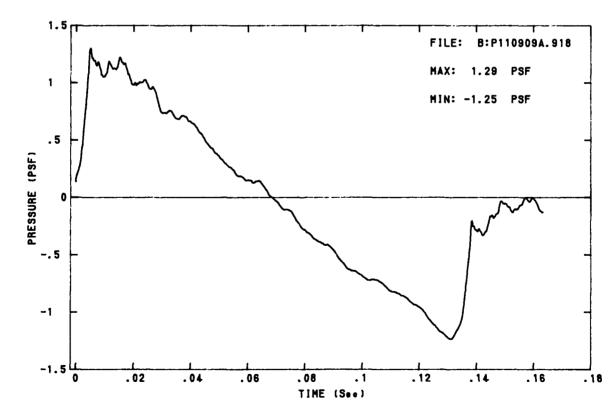
BOOM SIGNATURES from F-4 Flying at 1.22 MACH, 34,200 ft AGL, and 0 ft. track offset occuring at 16:09 GMT, 18 Sep 86.



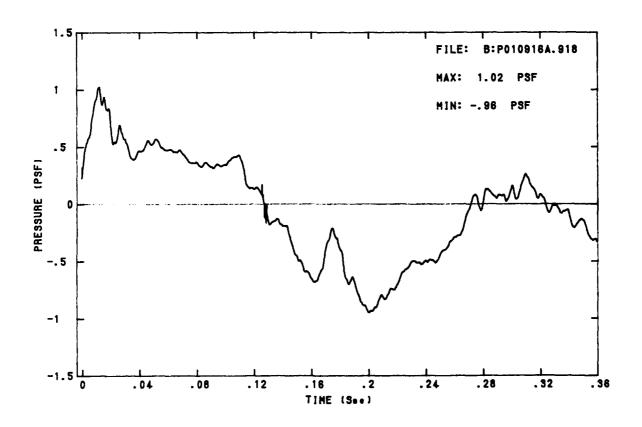


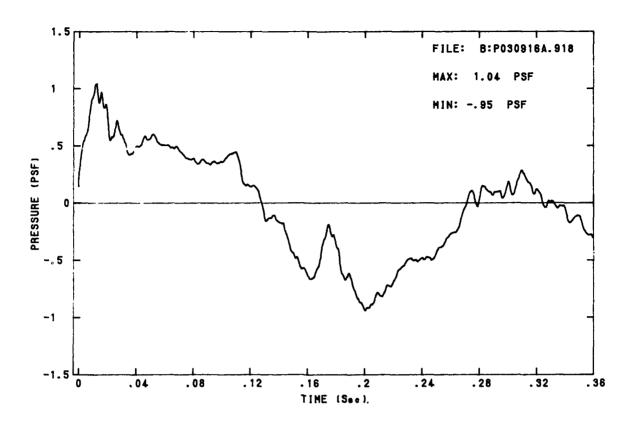


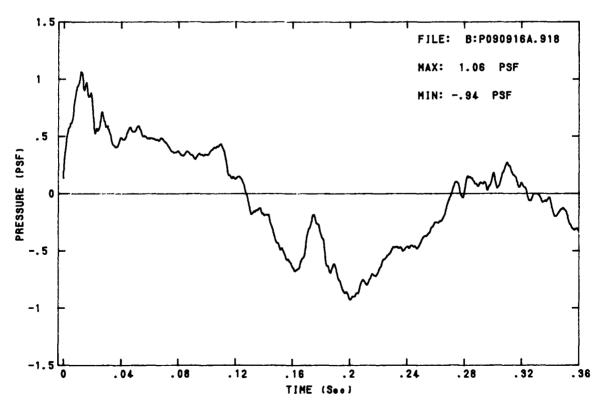


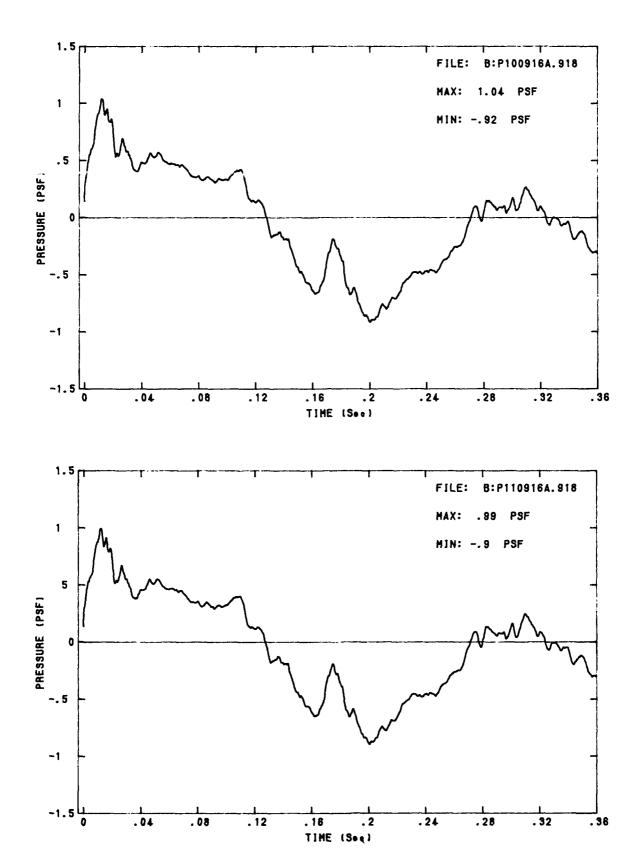


BOOM SIGNATURES from F-4 Flying at 1.28 MACH, 32,900 ft AGL, and 0 ft. track offset occuring at 16:16 GMT, 18 Sep 86.

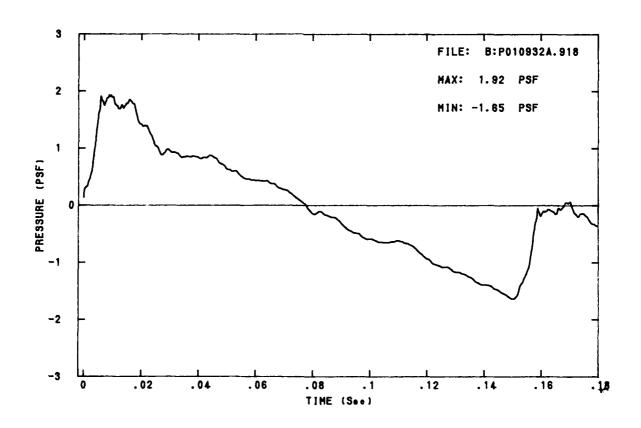


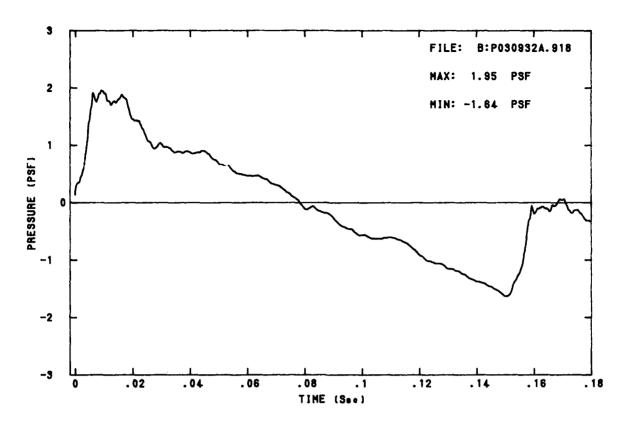


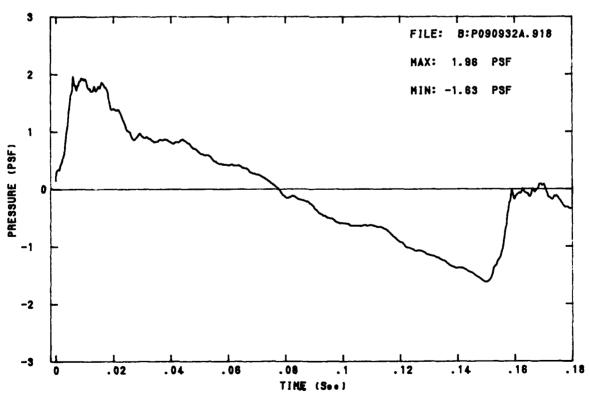


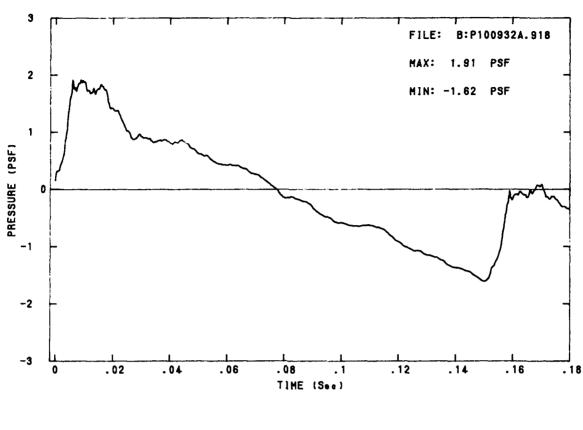


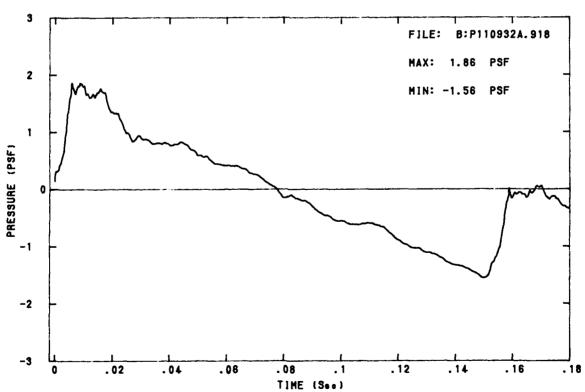
BOOM SIGNATURES from F-4 Flying at 1.35 MACH, 34,100 ft AGL, and 0 ft. track offset occuring at 16:32 GMT, 18 Sep 86.



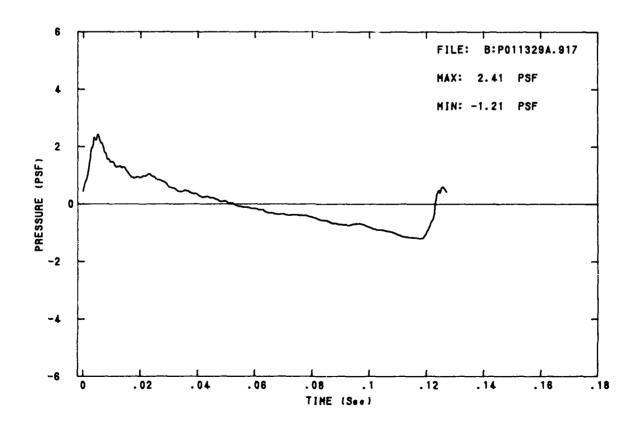


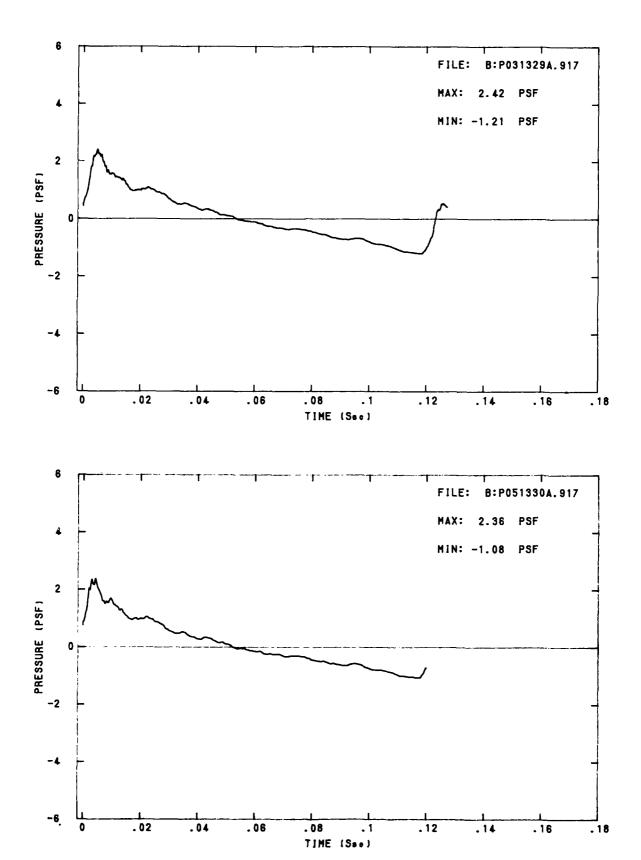


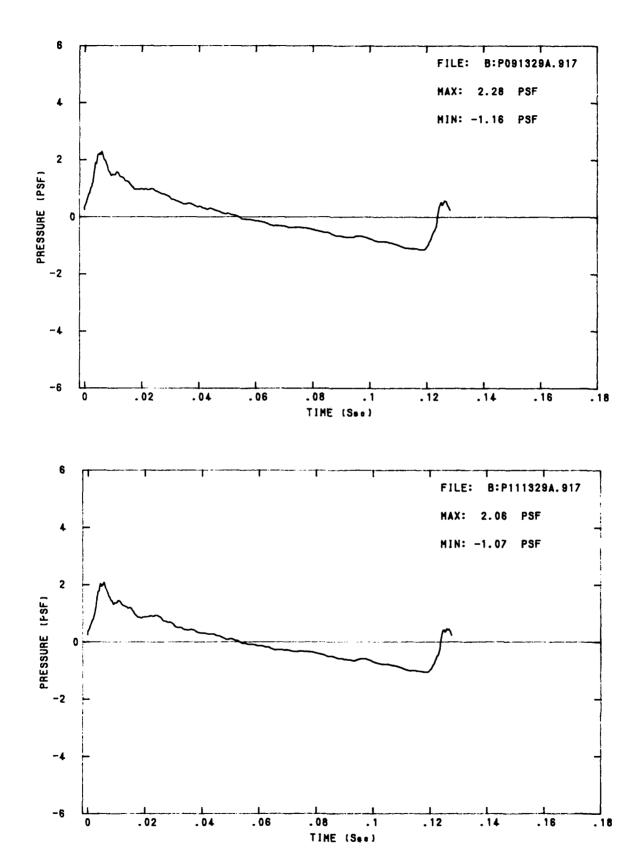




BOOM SIGNATURES from Unidentified Aircraft Occuring at 20:29 GMT, 17 Sep 86.



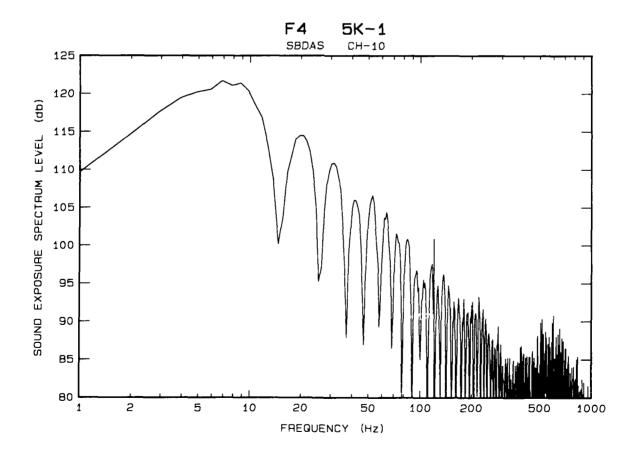


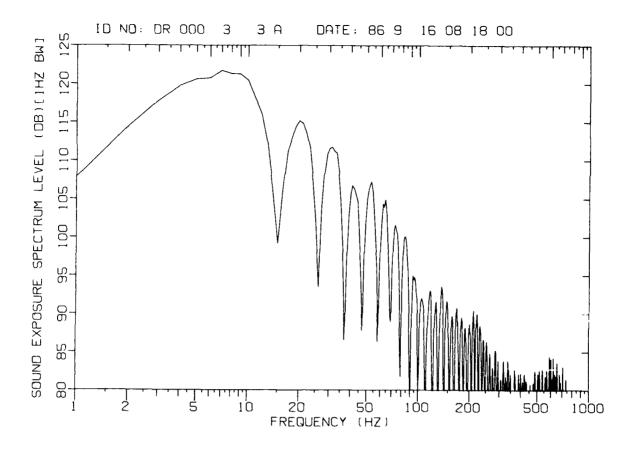


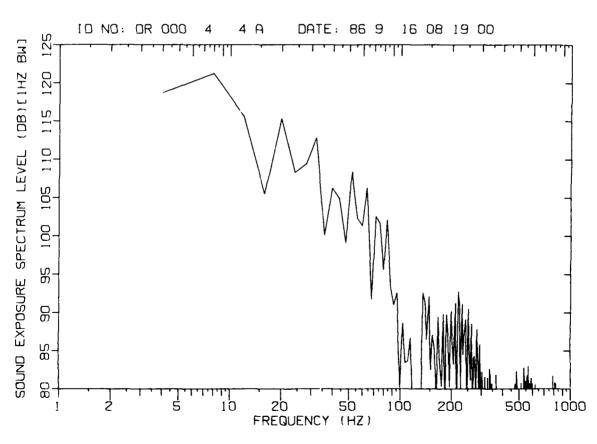
APPENDIX B

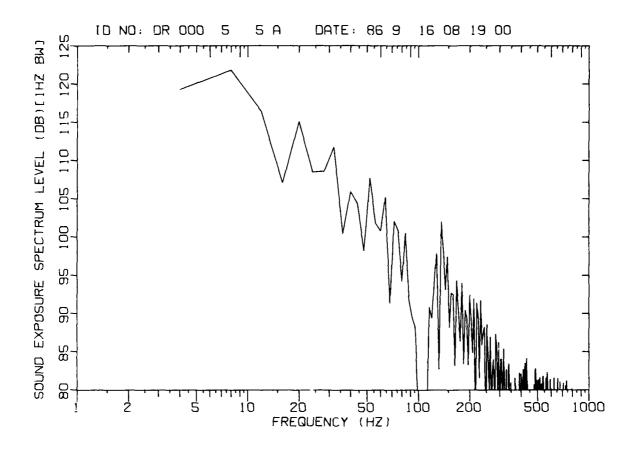
BOOM SPECTRUM LEVELS

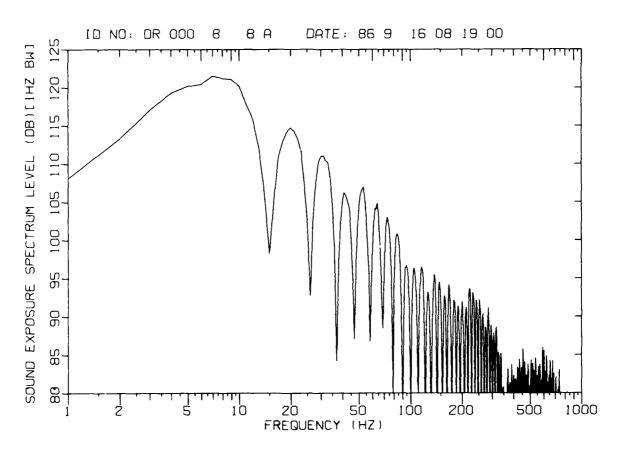
Sound Exposure Spectrum Level vs Frequency Plots of Sonic Boom from F-4 flying at 1.15 MACH, 6,000 ft. AGL, and 0 ft. track offset occuring at 15:20:08 GMT, 16 Sep 86.

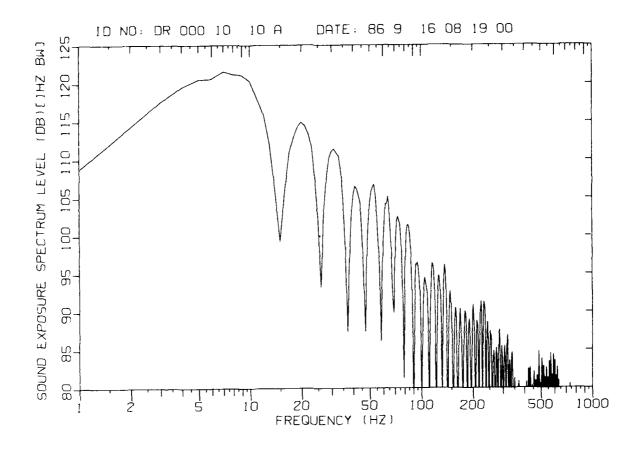


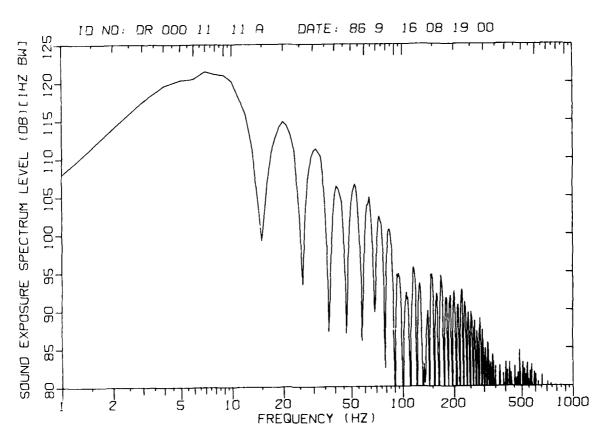


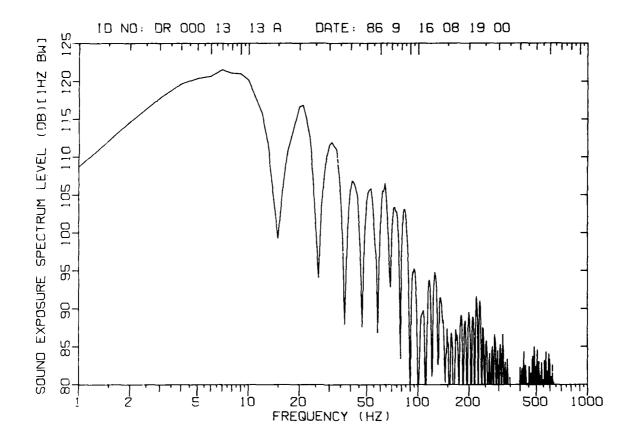




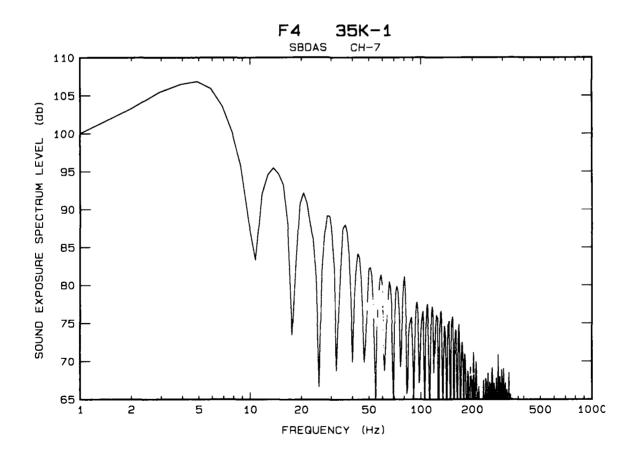


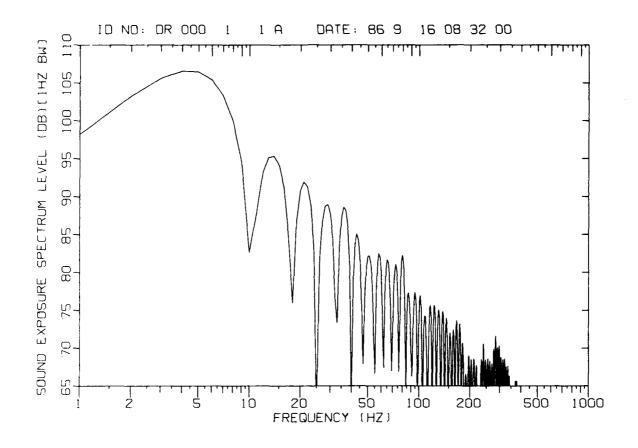


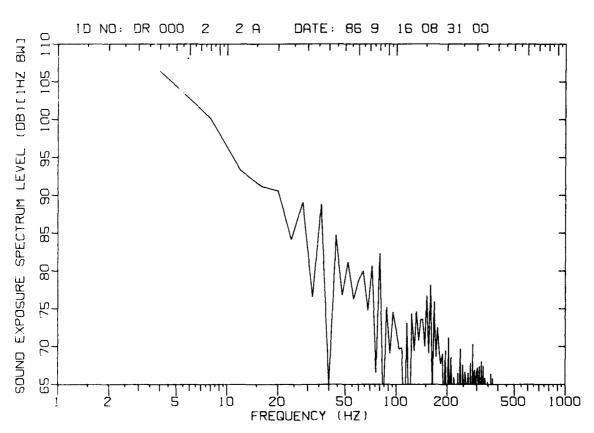


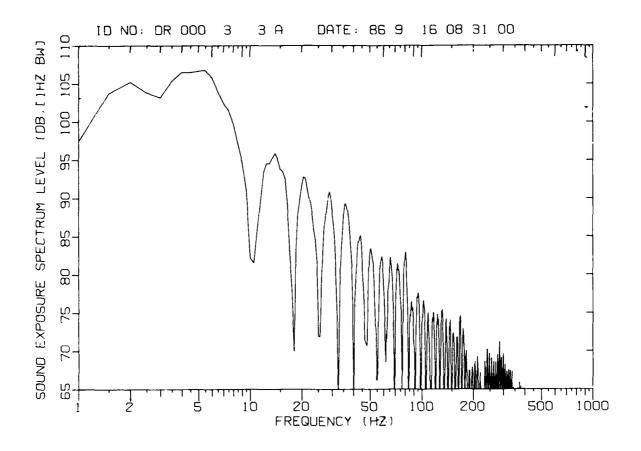


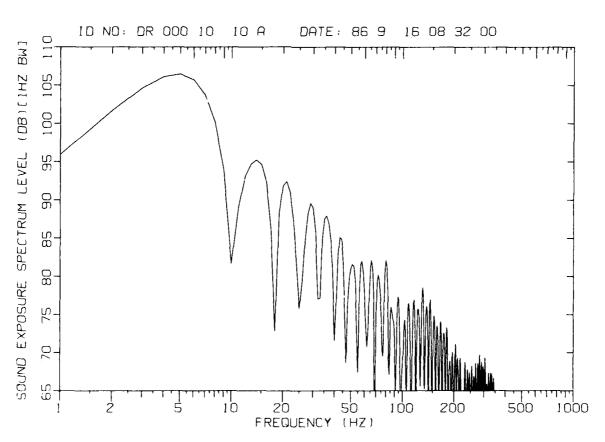
Sound Exposure Spectrum Level vs Frequency Plots of Sonic Boom from F-4 flying at 1.45 MACH, 35,000 ft. AGL, and 60,600 ft. track offset occuring at 15:33:04 GMT, 16 Sep 86.

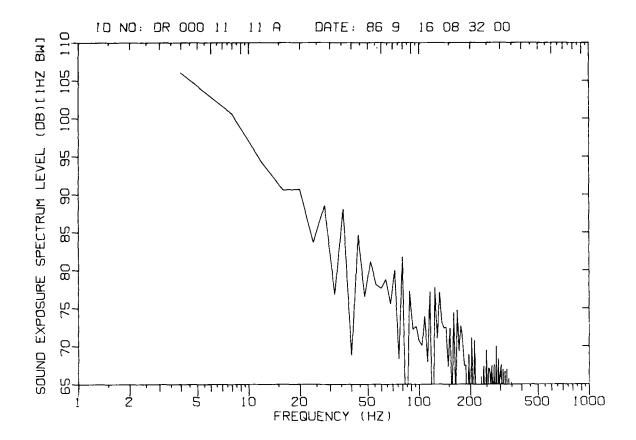




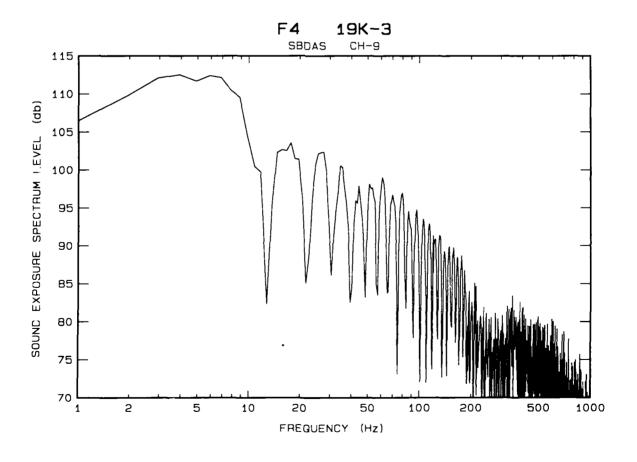


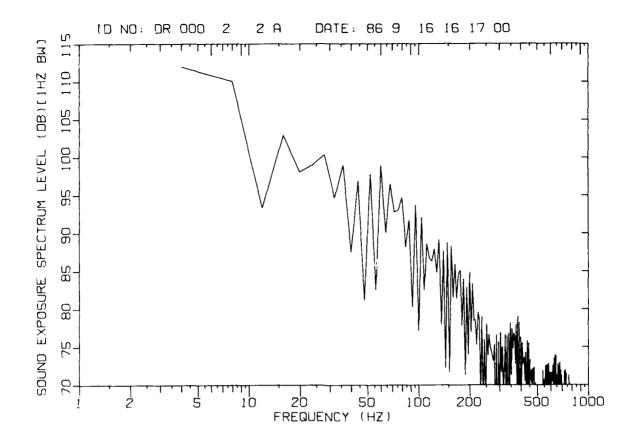


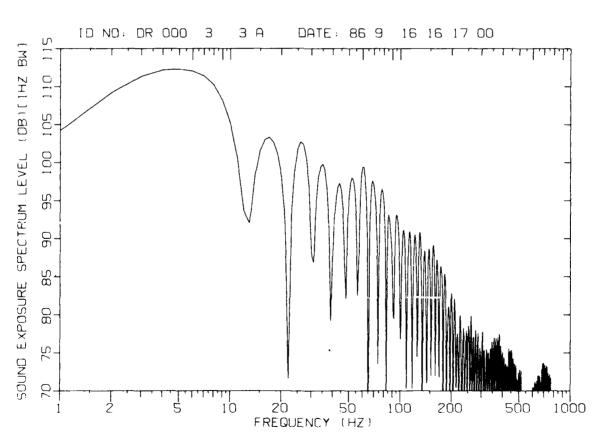


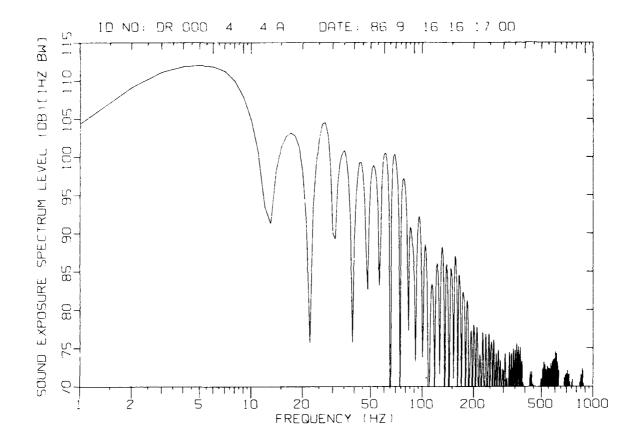


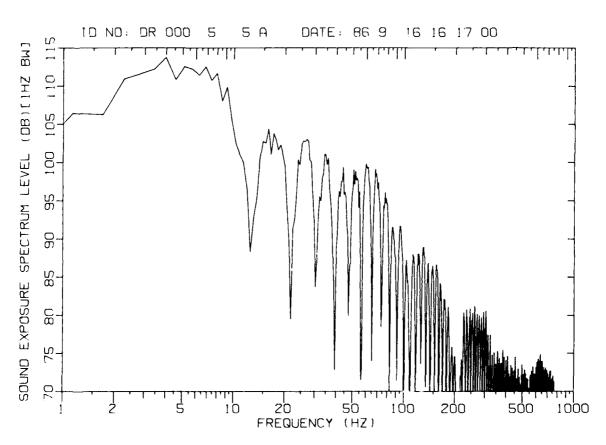
Sound Exposure Spectrum Level vs Frequency Plots of Sonic Boom from F-4 flying at 1.2 MACH, 25,700 ft. AGL, and 0 ft. track offset occuring at 23:17:47 GMT, 16 Sep 86.

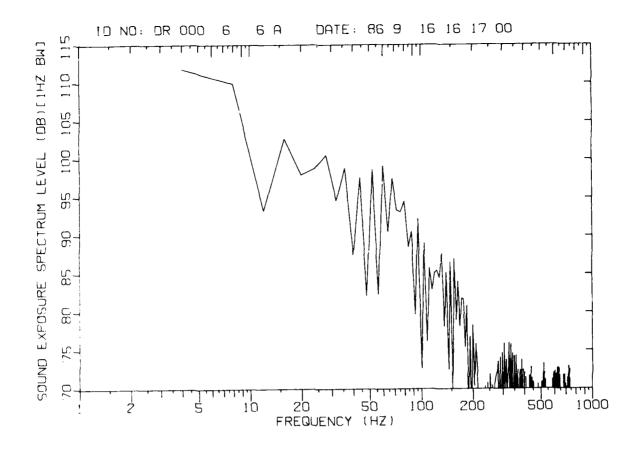


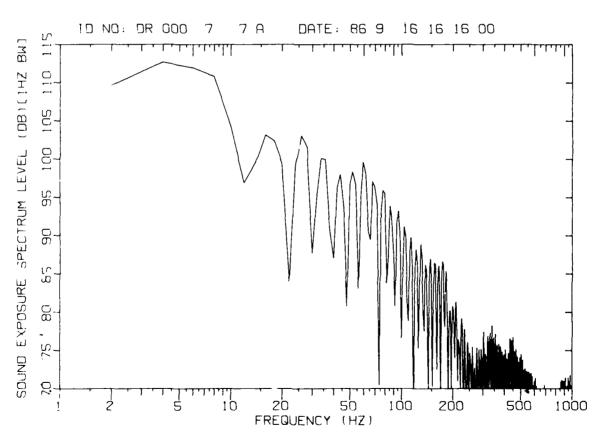


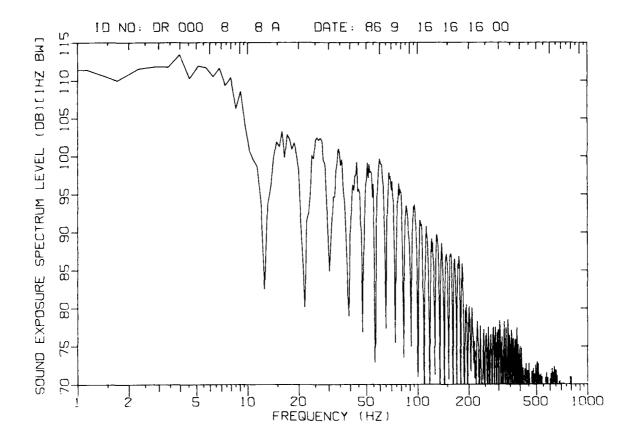


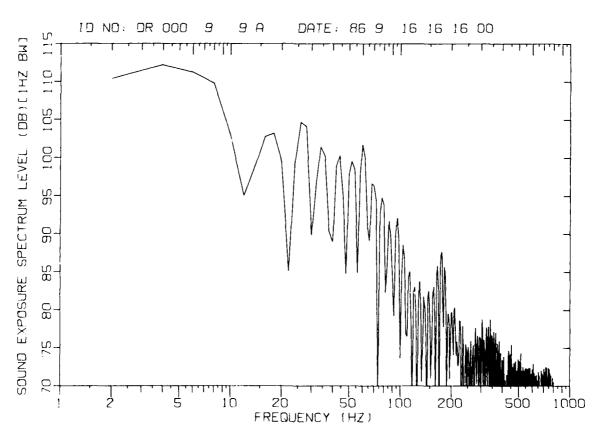


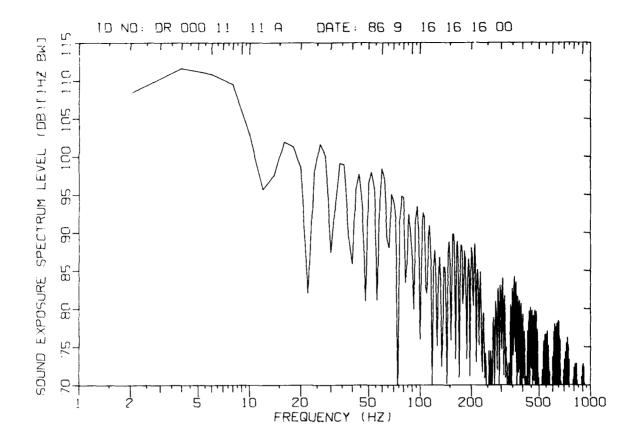


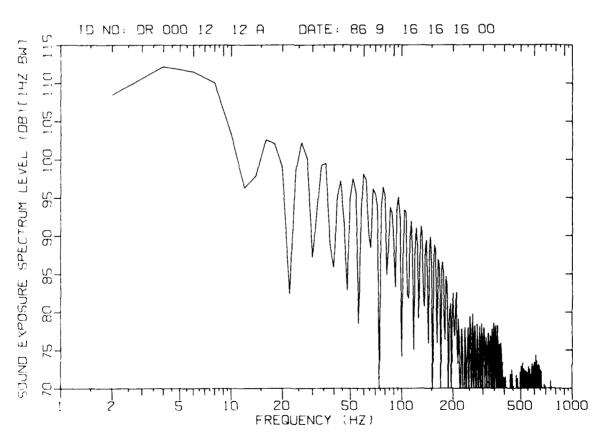


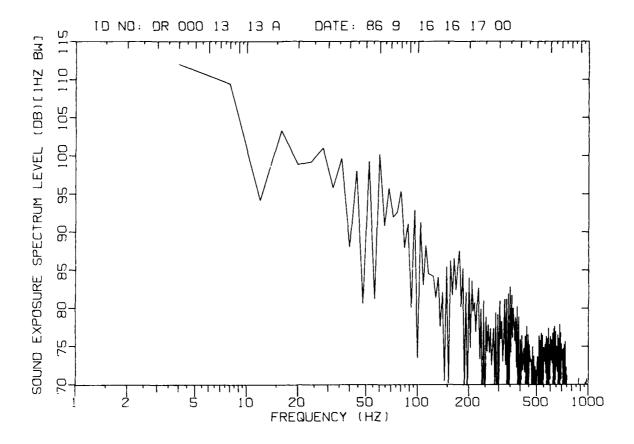




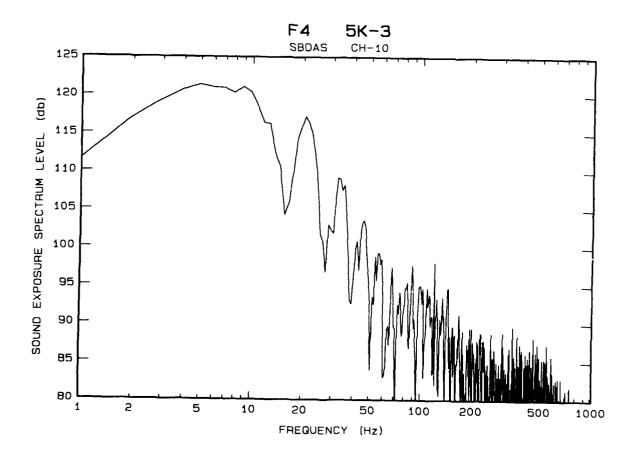


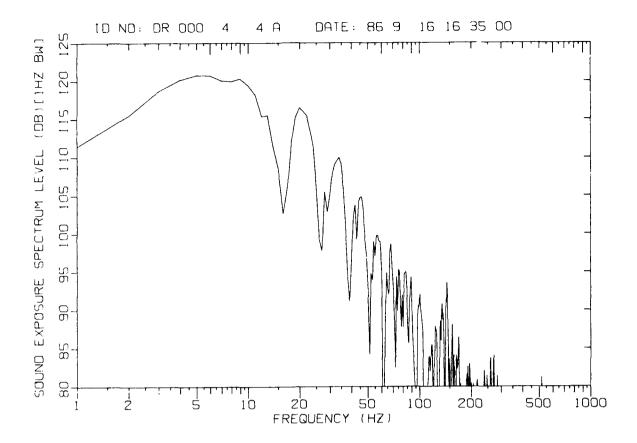


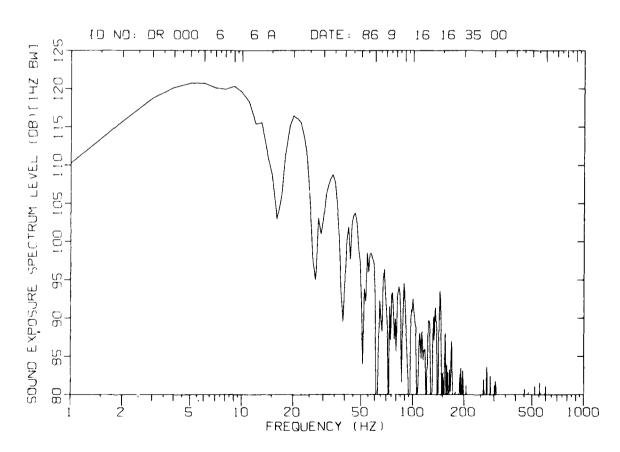




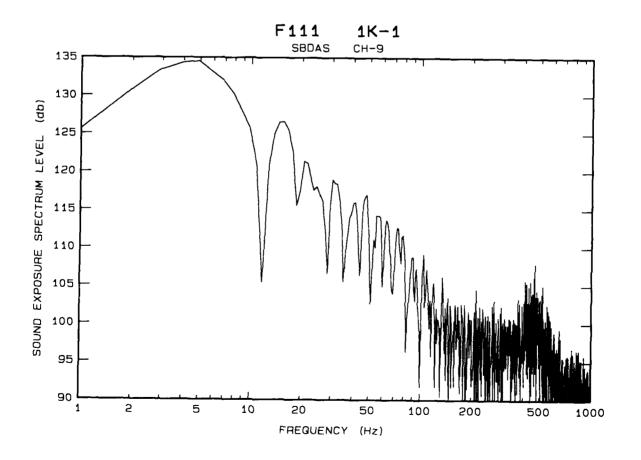
Sound Exposure Spectrum Level vs Frequency Plots of Sonic Boom from F-4 flying at 1.15 MACH, 5,200 ft. AGL, and 0 ft. track offset occuring at 23:35:18 GMT, 16 Sep 86.

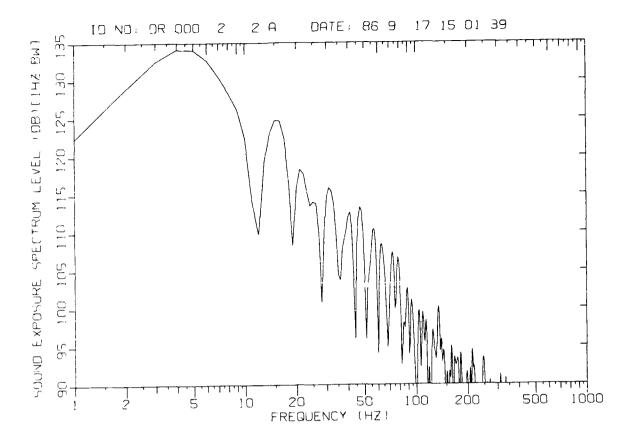


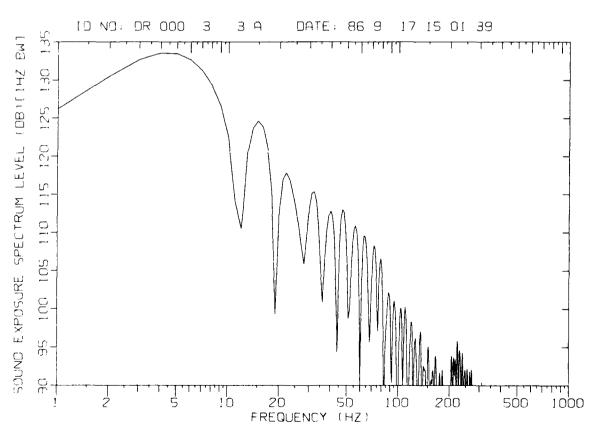


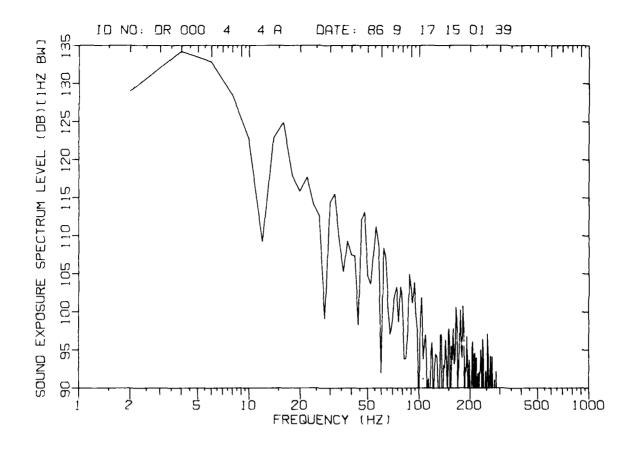


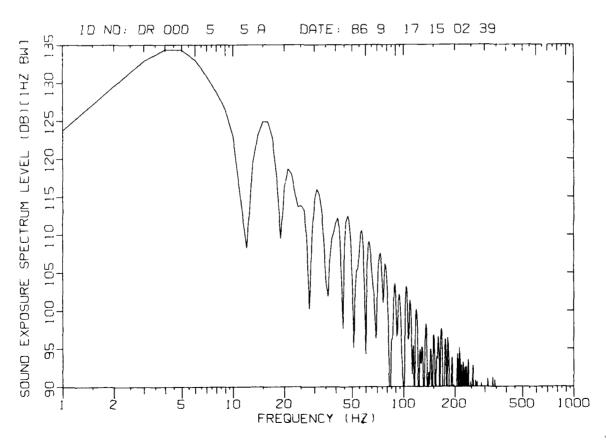
Sound Exposure Spectrum Level vs Frequency Plots of Sonic Boom from F-111A flying at 1.03 MACH, 1,200 ft. AGL, and 0 ft. track offset occuring at 22:02:33 GMT, 17 Sep 86.

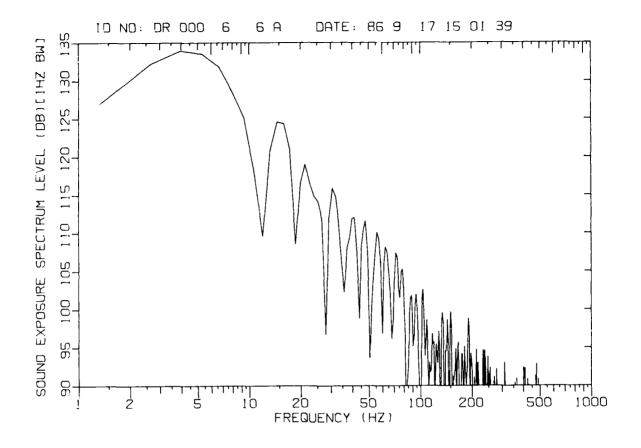


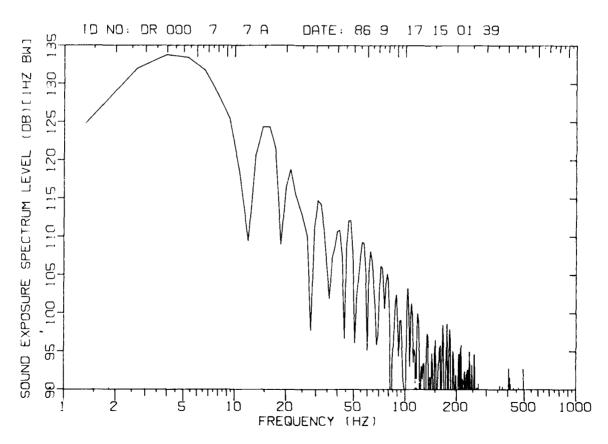


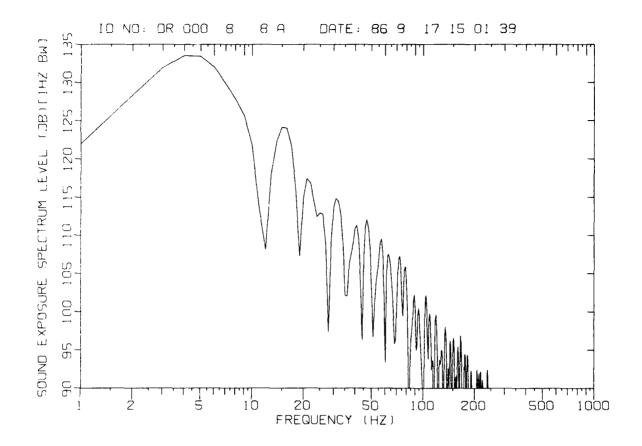












APPENDIX C

SINGLE METRIC TABLE

| *************** | | | | | | | | | |
|---|--|---|---|--|--|--|--------------------------------------|--|--|
| | | | 1. | 16 SEPT | 86 | 8:12 | am | | |
| BEAR SN | DISCR | IPTION | PEAK | DURATION | ASEL | CSEL | FSEL | | |
| 1 | FLUSH | MOUNT | 137.6 | 1.233 | 96.7 | 112.4 | 124.3 | | |
| 2 | FLUSH | MOUNT | | | | | | | |
| 3 | FLUSH | MOUNT | 138.0 | 1.342 | 96.2 | 113.0 | 124.4 | | |
| | FLUSH | | | | | | | | |
| | FLUSH | | 139.3 | 1.400 | 96.8 | 113.9 | 124.8 | | |
| | FLUSH | | | | | | | | |
| | FLUSH | | 138.6 | Ø . 138 | | 113.5 | | | |
| | FLUSH | | 137.3 | Ø.127 | | | | | |
| | FLUSH | | 137.7 | Ø.138 | | | | | |
| | FLUSH | | 137.5 | Ø . 129 | 96.2 | 113.1 | 124.4 | | |
| | FLUSH | | | | | | | | |
| | FLUSH | | | | | | | | |
| 13 | FLUSH | MOUNT | 138.5 | Ø.22Ø | 96.2 | 113.4 | 124.3 | | |
| ************************************** | | | | | | | | | |
| | | | _ | | | | | | |
| | | | 2. | 16 SEPT | 86 | 8:19 | am | | |
| BEAR SN | | | 2. PEAK | 16 SEPT DURATION | | 8:19 CSEL | | | |
| 1 | FLUSH | MOUNT | | | | | am | | |
| 1 2 | FLUSH FLUSH | MOUNT MOUNT | PEAK | | | | am | | |
| 1 2 3 | FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT | PEAK | DURATION Ø.857 | ASEL | CSEL 122.5 | am FSEL 131.5 | | |
| 1 2 3 4 | FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT | PEAK 146.8 148.0 | DURATION 0.857 0.190 | ASEL 106.4 105.6 | CSEL 122.5 123.4 | FSEL 131.5 131.5 | | |
| 1 2 3 4 5 | FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT MOUNT | PEAK | DURATION Ø.857 | ASEL 106.4 105.6 | CSEL 122.5 123.4 | FSEL 131.5 131.5 | | |
| 1 2 3 4 5 6 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT | PEAK 146.8 148.0 | DURATION 0.857 0.190 | ASEL 106.4 105.6 | CSEL 122.5 123.4 | FSEL 131.5 131.5 | | |
| 1 2 3 4 5 6 7 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT | PEAK 146.8 148.0 147.8 | DURATION Ø.857 Ø.19Ø Ø.174 | ASEL 106.4 105.6 107.0 | CSEL 122.5 123.4 123.3 | FSEL 131.5 131.5 131.8 | | |
| 1 2 3 4 5 6 7 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT | PEAK 146.8 148.0 | DURATION 0.857 0.190 | ASEL 106.4 105.6 107.0 | CSEL 122.5 123.4 123.3 | FSEL 131.5 131.5 | | |
| 1 2 3 4 5 6 7 8 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT MOUNT | PEAK 146.8 148.0 147.8 | DURATION Ø.857 Ø.19Ø Ø.174 | ASEL 106.4 105.6 107.0 | CSEL 122.5 123.4 123.3 | FSEL 131.5 131.5 131.8 | | |
| 1 2 3 4 5 6 7 8 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT | PEAK 146.8 148.0 147.8 | DURATION Ø.857 Ø.19Ø Ø.174 | ASEL 106.4 105.6 107.0 | CSEL 122.5 123.4 123.3 | FSEL 131.5 131.5 131.8 | | |
| 1 2 3 4 5 6 7 8 9 | FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH FLUSH | MOUNT | PEAK 146.8 148.0 147.8 146.9 146.5 146.5 | DURATION 0.857 0.190 0.174 0.910 0.849 0.849 | ASEL 106.4 105.6 107.0 107.6 | CSEL 122.5 123.4 123.3 122.6 | FSEL 131.5 131.5 131.8 | | |
| 1 2 3 4 5 6 7 8 9 10 | FLUSH | MOUNT | PEAK 146.8 148.0 147.8 146.9 | DURATION 0.857 0.190 0.174 0.910 0.849 0.849 | ASEL 106.4 105.6 107.0 107.6 | CSEL 122.5 123.4 123.3 122.6 | FSEL 131.5 131.5 131.8 131.4 | | |
| 1 2 3 4 5 6 7 8 9 10 11 12 | FLUSH | MOUNT | PEAK 146.8 148.0 147.8 146.9 146.5 146.5 | DURATION 0.857 0.190 0.174 0.910 0.849 0.849 | 106.4 105.6 107.0 107.6 106.1 106.3 | CSEL 122.5 123.4 123.3 122.6 122.6 122.4 | FSEL 131.5 131.5 131.8 131.4 131.3 | | |

```
16 SEPT 86
                                          8:32
BEAR SN DISCRIPTION
                   PEAK
                           DURATION
                                      ASEL
                                            CSEL
                                                   FSEL
      1 FLUSH MOUNT
                     126.7
                              0.189
                                      83.7
                                           100.9
                                                 114.0
      2 FLUSH MOUNT
                     126.9
                              Ø.188
                                      84.3 101.0 114.0
      3 FLUSH MOUNT
                     126.3
                              0.604
                                     83.2 100.9 114.0
      4 FLUSH MOUNT
      5 FLUSH MOUNT
      6 FLUSH MOUNT
     7 FLUSH MOUNT
     8 FLUSH MOUNT
     9 FLUSH MOUNT
     10 FLUSH MOUNT
                     126.8
                              Ø.218
                                     84.0 101.0 113.8
     11 FLUSH MOUNT
                     127.2
                              0.162
                                     83.8 100.9 113.8
     12 FLUSH MOUNT
                     126.8 *
     13 FLUSH MOUNT
*****************
                    4.
                           16 SEPT 86
                                          16:17 pm
BEAR SN DISCRIPTION
                    PEAK
                           DURATION
                                     ASEL
                                            CSEL
                                                   FSEL
     1 FLUSH MOUNT
                           DATA LOST DURING TRANSFER
     2 FLUSH MOUNT
                     139.1
                             Ø.245
                                     98.6 114.0 121.7
     3 FLUSH MOUNT
                     139.3
                              0.245
                                     97.5 114.0 121.8
     4 FLUSH MOUNT
                     139.4
                              Ø.252
                                     96.6
                                           114.7
                                                  121.9
     5 FLUSH MOUNT
                     138.9
                             1.504
                                     96.9
                                           113.8 121.9
     6 FLUSH MOUNT
                     139.Ø
                             Ø.249
                                     96.6
                                           113.7 121.5
     7 FLUSH MOUNT
                     140.3
                                           114.3 122.1
                             Ø.399
                                    100.3
     8 FLUSH MOUNT
                     138.7
                             1.614
                                     97.0
                                           113.8 121.5
     9 FLUSH MOUNT
                     138.6
                             Ø.432
                                     97.6
                                           114.8 122.0
    10 FLUSH MOUNT
                     138.9
                             1.504
                                     98.8
                                           114.0 121.7
    11 FLUSH MOUNT
                     138.2
                             Ø.485
                                    100.6
                                           113.9 121.1
    12 FLUSH MOUNT
                     138.7
                             0.483
                                     97.9
                                           114.0 121.5
    13 FLUSH MOUNT
                     138.7
                             0.177
                                    100.2 114.3 121.7
```

| ****** | ***** | ***** | **** | ***** | ***** |
|--|--------------------------------|--|---|--------------------------------------|------------------------|
| | 5. | 16 SEPT | 86 | 16:22 | pm |
| BEAR SN DISCRIPTION | PEAK | DURATION | | CSEL | |
| 1 FLUSH MOUNT | CA DOLLD | DATA LOS | | | PER |
| 2 FLUSH MOUNT 3 FLUSH MOUNT | 142.7 | ED WIND N | 96.0 | | 120 E |
| | 142.7 | | 90.0 | | |
| 4 FLUSH MOUNT 5 FLUSH MOUNT | 143.2 | 1.621 | 9/•0 | 11/.3 | 128.2 |
| 6 FLUSH MOUNT | 142.4 | 1 615 | 95.4 | 117 a | 120 5 |
| 7 FLUSH MOUNT | 142.4 | 1.013 | 95.4 | 11/.0 | 120.5 |
| 8 FLUSH MOUNT | | | | | |
| 9 FLUSH MOUNT | | | | | |
| 10 FLUSH MOUNT | | | | | |
| 11 FLUSH MOUNT | | | | | |
| 12 FLUSH MOUNT | 141 9 | 1 256 | 97 1 | 116 8 | 128 4 |
| 13 FLUSH *: DUNT | | ED WIND N | | | 120.4 |
| 19 120011 3001 | CHI TOIL | LD WIND N | 0100 110 | M 4 Divi | |
| | | | | | |
| ****** | **** | ***** | ****** | ***** | ***** |
| | | | | | |
| ****** | ***** | | | | |
| ****** | | | **** | ***** | ***** |
| ****** | | ***** | **** | ***** | ***** |
| BEAR SN DISCRIPTION | 6. PEAK | ******** 16 SEPT DURATION | ****** 86 ASEL | ******* 16:35 CSEL | pm ****** |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT | 6. PEAK | ******** 16 SEPT DURATION | ****** 86 ASEL | ******* 16:35 CSEL | pm ****** |
| BEAR SN DISCRIPTION | 6. PEAK | ******** 16 SEPT DURATION | ****** 86 ASEL | ******* 16:35 CSEL | pm ****** |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT | 6. PEAK DATA LO | ******** 16 SEPT DURATION OST DURIN | ****** 86 ASEL G TRANSI | ****** 16:35 CSEL FER | ****** pm FSEL |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT | 6. PEAK DATA LO | ******** 16 SEPT DURATION | ****** 86 ASEL G TRANSI | ****** 16:35 CSEL FER | ****** pm FSEL |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT | PEAK DATA LO | 16 SEPT DURATION OST DURIN | ******* 86 ASEL G TRANSI 101.6 | ******* 16:35 CSEL FER 121.2 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT | PEAK DATA LO | ******** 16 SEPT DURATION OST DURIN | ******* 86 ASEL G TRANSI 101.6 | ******* 16:35 CSEL FER 121.2 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT | PEAK DATA LO | 16 SEPT DURATION OST DURIN | ******* 86 ASEL G TRANSI 101.6 | ******* 16:35 CSEL FER 121.2 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT | PEAK DATA LO | 16 SEPT DURATION OST DURIN | ******* 86 ASEL G TRANSI 101.6 | ******* 16:35 CSEL FER 121.2 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT 10 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN 0.993 | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT 10 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN 0.993 | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT 10 FLUSH MOUNT 11 FLUSH MOUNT 12 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN 0.993 | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT 10 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN 0.993 | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |
| BEAR SN DISCRIPTION 1 FLUSH MOUNT 2 FLUSH MOUNT 3 FLUSH MOUNT 4 FLUSH MOUNT 5 FLUSH MOUNT 6 FLUSH MOUNT 7 FLUSH MOUNT 8 FLUSH MOUNT 9 FLUSH MOUNT 10 FLUSH MOUNT 11 FLUSH MOUNT 12 FLUSH MOUNT | 6. PEAK DATA LO 146.5 145.5 | 16 SEPT DURATION OST DURIN 0.993 | ******** 86 ASEL G TRANSI 101.6 102.4 | ******* 16:35 CSEL FER 121.2 120.8 | ******** pm FSEL 131.2 |

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| | | | 7. | 17 | SEPT | 86 | 13:29 | pm |
| BEAR S | SN | DISCRIPTION | PEAK | DUI | RATION | ASEL | CSEL | FSEL |
| | 1 | FLUSH MOUNT | 135.5 | | Ø.127 | 88.7 | 108.7 | 117.4 |
| | | FLUSH MOUNT | | | | | | |
| | | FLUSH MOUNT | 135.6 | | Ø . 127 | 88.5 | 108.6 | 117.6 |
| | | 45 T FLTTRK | 100 0 | | ~ | | | |
| | | 45 F FLTTRK | 135.5 | | Ø.12Ø | 91.2 | 108.2 | 117.1 |
| | | 45 T FLTTRK | | | | | | |
| | | 45 B FLTTRK BBE MOUNT | | | | | | |
| | | BBE MOUNT | 135.1 | | 0.129 | 86.7 | 108.1 | 117.2 |
| 1 | | BBE MOUNT | 133•1 | | | 30.7 | 10011 | 11/11 |
| | | BBE MOUNT | 134.8 | | Ø.128 | 87.6 | 107.9 | 117.0 |
| 1 | L 2 | BBE MOUNT | | | | | | |
|] | 3 | BBE MOUNT | SYSTEM | MAI | LFUNCT: | IONING | (break : | in cable |
| | | | | | | | | |
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| ***** | ** | ****** | ****** 8. | | ***** SEPT | | | ****** pm |
| | | | 8. | 17 | SEPT | 86 | 14:11 | pm |
| | SN | DISCRIPTION | | 17 | | 86 ASEL | 14:11 CSEL | pm |
| | SN 1 | DISCRIPTION FLUSH MOUNT | 8. PEAK | 17 | SEPT RATION | 86 ASEL 89.4 | 14:11 CSEL 109.0 | pm FSEL |
| BEAR S | SN 1 2 | DISCRIPTION FLUSH MOUNT | 8. PEAK 135.0 | 17 | SEPT RATION Ø.227 | ASEL 89.4 108.3 91.1 | CSEL 109.0 115.6 109.4 | FSEL 122.0 123.1 122.2 |
| BEAR S | 5N 1 2 3 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK | 8. PEAK 135.0 137.2 135.6 135.4 | 17 | SEPT RATION Ø.227 Ø.332 Ø.228 Ø.270 | ASEL 89.4 108.3 91.1 92.4 | CSEL 109.0 115.6 109.4 109.5 | FSEL 122.0 123.1 122.2 122.2 |
| BEAR S | SN 1 2 3 4 5 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK | PEAK 135.0 137.2 135.6 135.4 135.3 | 17 | SEPT RATION Ø.227 Ø.332 Ø.228 Ø.27Ø Ø.119 | ASEL 89.4 108.3 91.1 92.4 92.5 | CSEL 109.0 115.6 109.4 109.5 109.0 | FSEL 122.0 123.1 122.2 122.2 122.3 |
| BEAR S | SN 1 2 3 4 5 6 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 T FLTTRK | 8. PEAK 135.0 137.2 135.6 135.4 135.3 135.4 | 17 | SEPT RATION 0.227 0.332 0.228 0.270 0.119 0.227 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 | Pm FSEL 122.0 123.1 122.2 122.2 122.3 122.0 |
| BEAR S | SN 1 2 3 4 5 6 7 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 T FLTTRK 45 B FLTTRK | PEAK 135.0 137.2 135.6 135.4 135.3 | 17 | SEPT RATION Ø.227 Ø.332 Ø.228 Ø.27Ø Ø.119 Ø.227 Ø.119 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 | FSEL 122.0 123.1 122.2 122.3 122.0 121.7 |
| BEAR S | SN 1 2 3 4 5 6 7 8 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 T FLTTRK 45 B FLTTRK BBE MOUNT | PEAK 135.0 137.2 135.6 135.4 135.3 135.4 | 17 | SEPT RATION 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 | FSEL 122.0 123.1 122.2 122.3 122.0 121.7 121.3 |
| BEAR S | SN 1 2 3 4 5 6 7 8 9 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 T FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT | 8. PEAK 135.0 137.2 135.6 135.4 135.3 135.4 135.3 134.7 135.2 | 17 | SEPT 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 0.330 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 89.6 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 109.2 | FSEL 122.0 123.1 122.2 122.2 122.3 122.0 121.7 121.3 121.9 |
| BEAR S | N 1 2 3 4 5 6 7 8 9 Ø | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 B FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT | PEAK 135.0 137.2 135.6 135.4 135.3 135.4 | 17 | SEPT RATION 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 89.6 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 109.2 | FSEL 122.0 123.1 122.2 122.2 122.3 122.0 121.7 121.3 121.9 |
| BEAR S | SN 1 2 3 4 5 6 7 8 9 0 1 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 B FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT BBE MOUNT BLE MOUNT | 8. PEAK 135.0 137.2 135.6 135.4 135.3 135.4 135.3 134.7 135.2 | 17 | SEPT 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 0.330 | ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 89.6 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 109.2 | FSEL 122.0 123.1 122.2 122.2 122.3 122.0 121.7 121.3 121.9 |
| BEAR S | N 1 2 3 4 5 6 7 8 9 Ø L1 2 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 B FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT | 8. PEAK 135.0 137.2 135.6 135.4 135.3 135.4 135.3 134.7 135.2 135.0 | 17 DUI | SEPT RATION 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 0.330 0.225 | 86 ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 89.6 90.2 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 109.2 108.8 | FSEL 122.0 123.1 122.2 122.2 122.3 122.0 121.7 121.3 121.9 |
| BEAR S | N 1 2 3 4 5 6 7 8 9 Ø L1 2 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 B FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT BBE MOUNT BLE MOUNT | 8. PEAK 135.0 137.2 135.6 135.4 135.3 135.4 135.3 134.7 135.2 135.0 | 17 DUI | SEPT RATION 0.227 0.332 0.228 0.270 0.119 0.227 0.119 0.163 0.330 0.225 | 86 ASEL 89.4 108.3 91.1 92.4 92.5 91.8 92.2 89.8 89.6 90.2 | CSEL 109.0 115.6 109.4 109.5 109.0 109.3 108.4 108.5 109.2 108.8 | FSEL 122.0 123.1 122.2 122.3 122.0 121.7 121.3 121.9 121.6 |

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| | | | 9. | 17 | SEPT | 86 | 14:20 | pm | |
| BEAR | 1 | DISCRIPTION FLUSH MOUNT FLUSH MOUNT | PEAK | DUI | RATION | ASEL | CSEL | FSEL | |
| | 4 | FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK | 126.6 | | Ø.134 | 84.9 | 99.7 | 112.7 | |
| | 7 8 9 10 11 12 | 45 T FLTTRK 45 B FLTTRK BBE MOUNT BBE MOUNT BBE MOUNT BBE MOUNT BBE MOUNT | | | | 85.2 | | 112.9 | |
| | 13 | BBE MOUNT | SYSTEM | MAI | LFUNCT: | IONING | (break : | in cable | |
| **** | *** | ***** | ***** | *** | ***** | ***** | ***** | ***** | |
| **** | k 1. * 1 | ***** | ***** | *** | ***** | ***** | | | |
| | | | 10. | 17 | SEPT | 86 | 14:25 | pm | |
| BEAR | 1 2 3 4 5 6 7 8 | FLUSH MOUNT FLUSH MOUNT 45 T FLTTRK 45 F FLTTRK 45 T FLTTRK 45 B FLTTRK BBE MOUNT | PEAK 123.8 | | RATION Ø.186 | | CSEL 98.9 | | |
| | 10 11 12 | BBE MOUNT BBE MOUNT BBE MOUNT | 124.1 | | Ø.181 | 80.2 | 99.0 | 107.8 | |
| | 13 | BBE MOUNT | SYSTEM | MAI | LFUNCT: | IONING | (break | in cable | |

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                  11.
                        17 SEPT 86
                                       14:30 pm
BEAR SN DISCRIPTION
                 PEAK
                        DURATION
                                        CSEL
                                 ASEL
                                               FSEL
                  147.5
                           Ø.538 1Ø5.9 124.3 131.9
     1 FLUSH MOUNT
     2 FLUSH MOUNT
                  148.2
                           Ø.155 108.2 124.6 132.0
     3 FLUSH MOUNT
     4 45 T FLTTRK
                  147.2
                           Ø.129 109.6 124.2 131.6
                           Ø.136 1Ø8.4 124.5 132.Ø
     5 45 F FLTTRK
                  146.8
                           Ø.204 108.7 124.3 131.9
     6 45 T FLTTRK
                  146.1
                         0.155 108.5 124.1 131.9
     7 45 B FLTTRK 146.3
                           Ø.53Ø 107.5 123.9 131.3
     8 BBE MOUNT
                   146.1
     9 BBE MOUNT
                   146.7
                           Ø.859 107.4 124.3 131.8
                           Ø.529 107.2 124.1 131.5
    10 BBE MOUNT
                 146.4
                  146.6
                           Ø.536 107.0 123.9 131.4
    11 BBE MOUNT
    12 BBE MOUNT
                   146.9
                           Ø.531 107.3 124.3 131.8
    13 BBE MOUNT
                  SYSTEM MALFUNCTIONING (break in cable
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                  12.
                        17 SEPT 86
                                       15:01 pm
BEAR SN DISCRIPTION PEAK DURATION ASEL
                                        CSEL
                                              FSEL
     1 FLUSH MOUNT
                           Ø.285 11Ø.3 128.Ø 141.5
     2 FLUSH MOUNT
                   154.1
                           Ø.193 108.7 127.9 141.5
     3 FLUSH MOUNT
                   153.9
                           Ø.278 1Ø9.8 127.7 141.4
     4 45 T FLTTRK
                   153.5
     5 45 F FLTTRK
                   153.8
                           Ø.278 108.8 128.0 141.8
     6 45 T FLTTRK
                   153.6
                           Ø.738 11Ø.5 127.9 141.6
                           Ø.742 11Ø.1 127.6 141.4
     7 45 B FLTTRK
                   153.3
                   152.7
                           Ø.287 107.5 127.1 140.9
     8 BBE MOUNT
     9 BBE MOUNT
    10 BBE MOUNT
    11 BBE MOUNT
    12 BBE MOUNT
    13 BBE MOUNT
                  SYSTEM MALFUNCTIONING (break in cable
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| | | | 13. | 17 | SEPT | 86 | 15:06 | pm |
| BEAR | | DISCRIPTION FLUSH MOUNT | PEAK | DUI | RATION | ASEL | CSEL | FSEL |
| | 2 | FLUSH MOUNT | 155.2 | | Ø.389 | 113.0 | 132.4 | 142.7 |
| | 3 | FLUSH MOUNT | 155.3 | | 0.437 | 116.0 | 133.0 | 142.8 |
| | 4 | 45 T FLTTRK | 155.3 | | 0.274 | 117.2 | 132.8 | 142.6 |
| | 5 | 45 F FLTTRK | 155.4 | | Ø.69Ø | 116.5 | 132.9 | 142.9 |
| | 6 | 45 T FLTTRK | 155.7 | | 0.942 | 118.7 | 133.4 | 143.0 |
| | 7 | 45 B FLTTRK | 155.4 | | 0.690 | 116.5 | 132.7 | 142.7 |
| | 8 | BBE MOUNT | 155.0 | | 1.433 | 117.8 | 132.3 | |
| | 9 | BBE MOUNT | | | | | | |
| | 10 | BBE MOUNT | 155.2 | | 1.226 | 114.8 | 132.6 | 142.5 |
| | 11 | BBE MOUNT | 155.9 | | 1.437 | 114.8 | 133.2 | 142.9 |
| | 12 | BBE MOUNT | 155.1 | | 1.435 | 114.9 | 132.5 | 142.6 |
| | 13 | BBE MOUNT | SYSTEM | MAI | FUNCT: | IONING | (break | in cable |
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| **** | *** | ***** | **** | *** | **** | ***** | ***** | ***** |
| | | | 14. | 18 | SEPT | 86 | 9:09 | am |
| BEAR | SN | DISCRIPTION | PEAK | DUI | RATION | ASEL | CSEL | FSEL |
| | | BBE MOUNT | 130.7 | | Ø.164 | 83.3 | 104.1 | 117.3 |
| | | BBE MOUNT | 130.3 | | Ø.154 | 82.4 | 103.7 | 117.2 |
| | | BBE MOUNT | 130.8 | | Ø.163 | 83.5 | 104.0 | 117.0 |
| | 10 | BBE MOUNT | 130.4 | | Ø.164 | 82.7 | 103.7 | 117.0 |
| | 11 | BBE MOUNT | 130.5 | | Ø.164 | 82.5 | 103.9 | 117.2 |

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| | | 15. | 18 SEPT | 86 | 9:16 | am |
| BEAR SN | DISCRIPTION | PEAK | DURATION | ASEL | CSEL | FSEL |
| 1 | BBE MOUNT | 128.1 | Ø.791 | 80.6 | 102.4 | 117.4 |
| 3 | BBE MOUNT | 128.1 | 0.795 | 80.9 | 102.3 | 117.3 |
| 9 | BBE MOUNT | 128.3 | 0.703 | 81.2 | 102.4 | 117.1 |
| 10 | BBE MOUNT | 128.1 | Ø.79Ø | 80.8 | 102.2 | 117.0 |
| 11 | BBE MOUNT | 128.2 | 0.790 | 81.0 | 102.4 | 117.3 |

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| | | | 16. | 18 | SEPT | 86 | 9:32 | am |
| BEAR SN | DISC | CRIPTION | PEAK | DUI | RATION | ASEL | CSEL | FSEL |
| 1 | BBE | MOUNT | 133.6 | | Ø.464 | 84.6 | 107.5 | 120.0 |
| 3 | BBE | MOUNT | 133.6 | | Ø.466 | 84.5 | 107.4 | 120.0 |
| 9 | BBE | MOUNT | 133.6 | | 0.465 | 85.3 | 107.4 | 119.8 |
| 10 | BBE | MOUNT | 133.4 | | 0.250 | 85.3 | 107.3 | 119.6 |
| 11 | EBE | MOUNT | 133.6 | | 0.465 | 85.5 | 107.5 | 119.9 |
